

Traffic Impact Study

St. Charles, Illinois

October 2021

Prepared for:

Casey's Retail Company









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EXECUTIVE SUMMARY

Kimley-Horn and Associates, Inc. (Kimley-Horn) was retained by Casey's Retail Company to perform a traffic impact study for the proposed Casey's General Store in St. Charles, Illinois. Access to the site will be provided by two full-movement driveways along Fieldgate Drive (Access A-B), as well as two internal driveways connecting the site to the surrounding shopping center.

As part of the traffic impact study, existing and future traffic conditions were evaluated for the unsignalized intersection of IL 64 and Fieldgate Drive. In addition, the proposed access points were evaluated for future build traffic conditions.

Based on a review of future traffic conditions, it is anticipated that the background traffic growth and the site-generated traffic would not materially impact the IL 64 corridor. The southbound approach at the intersection of IL 64 and Fieldgate Drive is projected to operate at LOS F under the Future Year 2027 Build traffic conditions in the PM and Saturday peak hours with 95th percentile queues of up to four vehicles. Low levels-of-service for side-street approaches are not uncommon, as vehicles may experience delays turning onto a major roadway. Additionally, there are many alternate route opportunities through the connectivity of the site to the surrounding shopping center and to adjacent signalized intersections on Foxfield Road accessible via Fieldgate Drive. This analysis may be conservative since outbound site traffic is likely to make an alternate route choice to avoid visible queues when exiting the site.

Limited delay and queues are anticipated at the site driveways in the future conditions. To facilitate site access and onsite circulation, minor-leg stop control should be posted for the outbound traffic at Access A and Access B. For the analysis of future traffic conditions, turn lane warrants were evaluated for the study intersections and the proposed site access driveways using guidelines in the IDOT *BDE Manual*. Based on the IDOT *BDE Manual* volume guidance provided for unsignalized intersections on two-lane facilities, projected future traffic volumes do not meet warrant criteria for a southbound left-turn lane or a northbound right-turn lane on Fieldgate Drive at Access A or a southbound left-turn lane at Access B. A northbound right-turn lane is warranted at Access B based on the *BDE Manual*. Per coordination with the City of St. Charles, Fieldgate Drive should be restriped to provide a northbound right-turn lane as its cross section is wide enough for two (2) lanes.

These study results are discussed in more detail in the *Recommendations & Conclusion* section of this report.



1. INTRODUCTION

Kimley-Horn and Associates, Inc., (Kimley-Horn) was retained by Casey's to perform a traffic impact study for a proposed Casey's General Store on the northeast corner of IL 64 and Fieldgate Drive in St. Charles, Illinois. The development is proposed to include 16 fueling positions and approximately 5,000 SF of convenience store space. The proposed site for the redevelopment was formerly used as a commercial development.

Access to the site will be provided by two full-movement driveways along Fieldgate Drive (Access A-B), as well as two internal access points connecting the site to the surrounding shopping center. An aerial view of the study location and surrounding roadway network is presented in **Exhibit 1**.

As part of this study, the existing roadway network was analyzed to determine the current operations at the study intersections. In order to assess the site's potential impact on the area roadway network, site generated trips were established and added to the background traffic volumes. Consistent with the Illinois Department of Transportation (IDOT) requirements, future traffic conditions were evaluated for Future Year 2027. This report presents and documents Kimley-Horn's data collection, summarizes the evaluation of existing and projected future traffic conditions on the surrounding roadways, and identifies recommendations to address the potential impact of site-generated traffic on the adjacent roadway network for the Future Year 2027 traffic conditions.



Kimley» Horn

EXHIBIT 1
SITE LOCATION MAP



2. EXISTING CONDITIONS

Based on aerial imagery as well as a site visit, Kimley-Horn conducted a review of the subject site including existing land uses in the surrounding area, the adjacent street system, current traffic volumes and operating conditions, lane configurations and traffic controls at nearby intersections, and other key roadway characteristics. This section of the report details information on the existing conditions.

Area Land Uses & Connectivity

Located on the northeast quadrant of the IL 64 and Fieldgate Drive intersection, the subject site is currently developed as a commercial site. The site is bound by IL 64 to the south, Fieldgate Drive to the west, and commercial properties to the north and east. Located in St. Charles, Illinois, the site is surrounded by residential and commercial land uses.

IL 64 provides regional connectivity to the east and west and Kirk Road provides regional connectivity to the north and south approximately 1,500 feet east of the project site.

Existing Roadway Characteristics

A field investigation was conducted within the study area. As a result of this visit, the following information was obtained about the existing roadway network.

IL 64 is an east-west roadway that runs along the southern frontage of the subject site. The Illinois Department of Transportation classifies IL 64 as a Principal Arterial. Through the study area, two travel lanes are provided in each direction, and dedicated left and right-turn lanes are provided at key intersections. At its unsignalized, minor-leg stop-controlled intersection with Fieldgate Drive, IL 64 provides two through lanes and a two-way left-turn lane (TWLTL) on both the east and west legs and a dedicated right-turn lane on the east leg of the intersection. There are several driveways serving existing commercial developments along the south side of IL 64 in the vicinity of its study intersection with Fieldgate Drive. A crosswalk is provided on the north leg of the intersection. IDOT classifies IL 64 as a Strategic Regional Arterial (SRA) roadway. The SRA system was established by IDOT to promote mobility on key routes throughout the Chicago area by applying various strategies, such as access control and limited signalization. A speed limit of 35 miles per hour (MPH) is posted on IL 64 through the study area. IL 64 is under IDOT jurisdiction.

Fieldgate Drive is a north-south roadway that runs along the western frontage of the subject site. Through the study area, Fieldgate Drive provides one travel lane in each direction. At its minor-leg stop-controlled intersection with IL 64, Fieldgate Drive provides dedicated left and right-turn lanes. At its minor-leg stop-controlled intersection with Access B, Fieldgate Drive provides one shared through/right-turn lane on the south leg and one shared left-turn/though lane on the north leg. A crosswalk is provided at the north leg of the intersection with IL 64. A speed limit of 25 MPH is posted on Fieldgate Drive through the study area. Fieldgate Drive is under the jurisdiction of the City of St. Charles.



Access B is an existing private driveway located approximately 100 feet north of the intersection of IL 64 and Fieldgate Drive. At its minor-leg stop-controlled intersection with Fieldgate Drive, Access B provides two inbound lanes and one dedicated left-turn lane and one dedicated right-turn lane outbound on the east leg.

Traffic Count Data

Turning movement count data was collected in March 2021 at the study intersection of IL 64 and Fieldgate Drive. The counts were conducted on a typical weekday from 7:00 to 9:00AM, and 4:00 to 6:00PM. Additionally, counts were conducted on a typical Saturday from 11:00AM to 1:00PM. These count periods were selected in order to capture peak travel periods in the area. The traffic count data indicates that peak traffic volumes occur within the study area from 7:15 to 8:15AM and 4:45 to 5:45PM on weekdays, and from 12:00PM to 1:00PM on Saturdays.

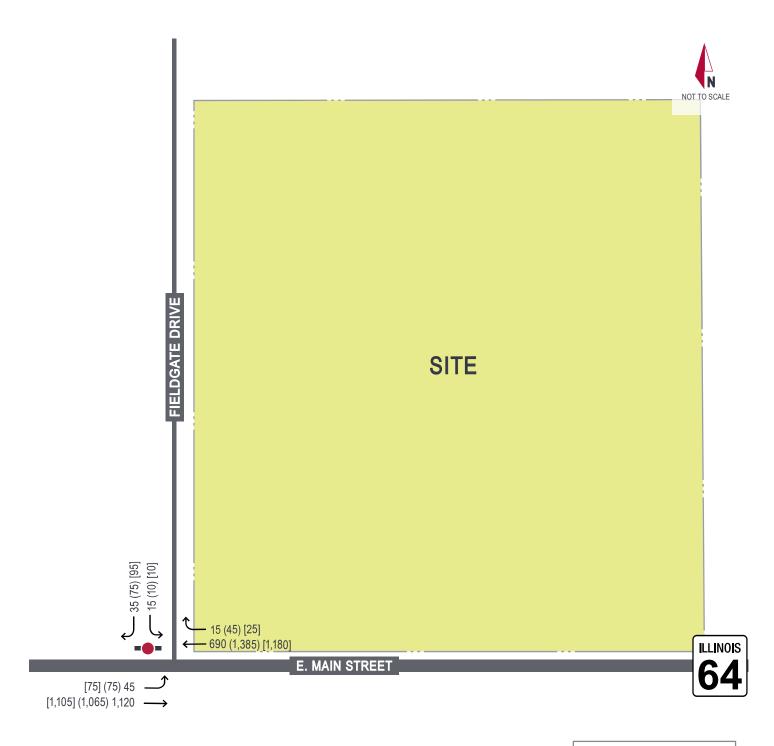
24-hour counts were additionally collected for the study intersection on Thursday, March 25, 2021. The 24-hour traffic counts for the study intersection were compared to historical IDOT count data in order to determine if there was an impact on the traffic patterns in the study area due to COVID-19. The collected March 2021 data was greater than the available 2019 IDOT data along IL 64. Based on the volume comparison, no adjustments were made to the existing 2021 traffic counts.

The peak hour vehicle traffic volumes were rounded to the nearest multiple of five. The existing traffic volumes are presented in **Exhibit 2**. A summary of the traffic count data is provided in the appendix.

Existing Capacity Analysis

Capacity analysis for the existing and future conditions was performed using Synchro Version 10. The capacity of an intersection quantifies its ability to accommodate traffic volumes and is expressed in terms of level of service (LOS), measured in average delay per vehicle. LOS grades range from A to F, with LOS A as the highest (best traffic flow and least delay), LOS E as saturated or at-capacity conditions, and LOS F as the lowest (oversaturated conditions). The lowest LOS grade typically accepted by jurisdictional transportation agencies in Northeastern Illinois is LOS D, and a minimum LOS C is required for through movements on SRA routes such as IL 64.

The LOS grades shown below, which are provided in the Transportation Research Board's <u>Highway Capacity Manual</u> (HCM), quantify and categorize the driver's discomfort, frustration, fuel consumption, and travel times experienced as a result of intersection control and the resulting traffic queuing. A detailed description of each LOS rating can be found in **Table 2.1**.



LEGEND

- **XX** Weekday AM Peak (7:15 8:15am)
- (**xx**) Weekday PM Peak (4:45 5:45pm)
- [**xx**] Saturday Peak (12:00 1:00pm)
- Existing Stop Sign
- Less than Five Vehicles



Table 2.1 Level of Service Grading Descriptions¹

Level of Service	Description
А	Minimal control delay; traffic operates at primarily free-flow conditions; unimpeded movement within traffic stream.
В	Minor control delay at signalized intersections; traffic operates at a fairly unimpeded level with slightly restricted movement within traffic stream.
С	Moderate control delay; movement within traffic stream more restricted than at LOS B; formation of queues contributes to lower average travel speeds.
D	Considerable control delay that may be substantially increased by small increases in flow; average travel speeds continue to decrease.
Е	High control delay; average travel speed no more than 33 percent of free flow speed.
F	Extremely high control delay; extensive queuing and high volumes create exceedingly restricted traffic flow.

¹Highway Capacity Manual, 6th Edition.

The range of control delay for each rating (as detailed in the HCM) is shown in **Table 2.2**. Because signalized intersections are expected to carry a larger volume of vehicles and stopping is required during red time, note that higher delays are tolerated for the corresponding LOS ratings.

Table 2.2 Level of Service Grading Criteria¹

Level of Service	Average Co	ntrol Delay (s/veh) at:
Level of Service	Unsignalized Intersections	Signalized Intersections
Α	0 – 10	0 – 10
В	> 10 – 15	> 10 – 20
С	> 15 – 25	> 20 – 35
D	> 25 – 35	> 35 – 55
Е	> 35 – 50	> 55 – 80
F ²	> 50	> 80

¹Highway Capacity Manual, 6th Edition

Based on these standards, capacity results were identified for the study intersections under existing conditions. The results of capacity analysis for existing conditions are summarized in **Table 2.3**. In this table, operation on each approach is quantified according to the average delay per vehicle and the corresponding level of service. The results are based on Synchro's HCM 6th Edition reports. Copies of the Synchro reports are provided in the appendix.

Table 2.3 Existing (2021) Levels of Service

	Weekday	AM Peak	Weekday F	PM Peak	Saturday Midday Peak		
Intersection	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	
IL 64 / Fieldgate Drive							
Southbound							
Left-Turn	20	С	41	E	32	D	
Right-Turn	11	В	18	С	16	С	
Approach	14	В	20	С	18	С	
Eastbound							
Left-Turn	9	Α	15+	С	13	В	

^{△-} Minor-Leg Stop-Controlled Intersection

²All movements with a Volume to Capacity (v/C) ratio greater than 1 receive a rating of LOS F.



At the minor-leg stop-controlled intersection of IL 64 and Fieldgate Drive, all approaches currently operate acceptably at LOS C or better for each of the AM, PM, and Saturday peak hours. For this study intersection, the 95th percentile queues estimates are approximately one vehicle (approximately 25 feet) or less for all approaches in each peak hour.



3. DEVELOPMENT CHARACTERISTICS

This section of the report outlines the proposed site plan, summarizes site-specific traffic characteristics, defines future roadway improvements, and develops future traffic projections for analysis.

Development Characteristics

The proposed development would include an approximately 5,000 SF convenience store with sixteen (16) vehicle fueling positions. The proposed site would include two full access driveways on Fieldgate Drive (Access A and Access B). Proposed Access A is located approximately 275 feet north of the intersection of IL 64 and Fieldgate Drive and would provide one inbound lane and two outbound lanes including one dedicated left-turn lane and one dedicated right-turn lane. Access A is necessary on the site to facilitate fuel truck operations. Access B is an existing private driveway to the commercial development on the project site located approximately 100 feet north of the intersection of IL 64 and Fieldgate Drive. Access B provides two inbound and two outbound lanes.

In addition to Access A and Access B, the proposed development includes two access points to the surrounding commercial developments via internal connections. The internal accesses were not analyzed in this traffic study. A conceptual site plan is provided in the appendix.

Trip Generation

In order to calculate trips generated by the proposed site, data was referenced from the Institute of Transportation Engineers (ITE) manual titled <u>Trip Generation</u>, <u>Tenth Edition</u>. Trip generation rates for the ITE Land Use Code (LUC) corresponding to the proposed use are shown in **Table 3.1**. A copy of the ITE data are provided in the appendix.

Table 3.1 ITE Trip Generation Data

ITE Land Use	Unit		Weekday										
THE LANGUSE	UTIIL	Daily	AM Peak Hour	PM Peak Hour	Midday Peak Hour								
Super Convenience Store/Gas Station (LUC) 960	Per vehicle fueling positions	230.52X 50% in/50% out	28.08X 50% in/50% out	22.96X 50% in/50% out	23.26X 50% in/50% out								

X = Vehicle Fueling Positions

For the purpose of this study, site generated trips are expected to exhibit multiple routing patterns when traveling to and from the subject site, as described below:

- Internal Trips The proposed redevelopment will be internally connected to the existing
 adjacent shopping center. It is likely that some patrons that visit the shopping center will also
 stop at the Casey's General Store. To reflect these internal trips, a 5 percent reduction was
 assumed to account for the trips between the existing shopping center and the proposed gas
 station/convenience store.
- Pass-by Pass-by traffic reflects the travel patterns of motorists who are already traveling on
 the adjacent study roadways and stop at the site en route to another destination. Data in the
 ITE <u>Trip Generation Handbook</u>, <u>Third Edition</u>, reveals that roughly 62 percent of vehicles at a
 Convenience Market with a Gas Station are pass-by trips in the weekday morning peak hour
 and 56 percent of vehicles are pass-by trips during the weekday evening peak hour. ITE data



- is not provided for daily and Saturday midday pass-by trips; therefore, the weekday evening pass-by percentage was applied (56 percent).
- **Primary Trips** Vehicles that travel to the subject development and then return directly to their place of origin are called "primary trips." Primary trips reflect new traffic volumes generated by the proposed development that would approach and depart on the same route. Trips to/from the site that are not pass-by trips are expected to be primary trips.

No existing traffic was removed from the network. **Table 3.2** shows the site generated traffic projections.

Table 3.2 Site-Generated Traffic Projections¹

		Daily			Wee	ekday			Saturday				
Land Use	Size		AM	l Peak H	our	PM	Peak Ho	our	Midday Peak Hour				
			ln	Out	Total	In	Out	Total	ln	Out	Total		
Super Convenience Market / Gas Station (LUC 960) 16 Fueling Positions		3,690	225	225	450	185	185	370	185	185	370		
Internal Shopping Center	r Trips	-180	-10	-10	-20	-10	-10	-20	-10	-10	-20		
Total Driveway Trips	Total Driveway Trips			215	430	175	175	350	175	175	350		
Pass-By Trips ²		-1,960	-135	-135	-270	-100	-100	-200	-100	-100	-200		
Net New Site Trips	1,550	80	80	160	75	75	150	75	75	150			

¹In/Out volumes are rounded to the nearest multiple of five.

Based on the connectivity of the proposed site to the surrounding commercial shopping center, the internal shopping center trips referenced in **Table 3.2** represent approximately 5% of the proposed site traffic which was assumed to interact directly with the adjacent shopping center. The internal shopping center trips were assumed to be completely contained by roadways internal to the development and shopping center and therefore do not create new trips at Access A-B.

Directional Distribution

The estimated distribution of site-generated traffic on the surrounding roadway network as it approaches and departs the site is a function of several variables, such as the nature of surrounding land uses, prevailing traffic volumes/patterns, characteristics of the street system, and the ease with which motorists can travel over various sections of that system. The anticipated directional distributions estimated for the primary trips and pass-by trips are outlined in **Table 3.3**.

²Based upon the ITE Trip Generation Handbook, Third Edition, pass-by trips for the site are assumed to be 62 percent during the weekday morning, 56 percent during the weekday evening. ITE data is not provided for Saturday midday and daily pass-by trips; therefore, the weekday evening pass-by percentage was applied.



Table 3.3 Estimated Trip Distribution

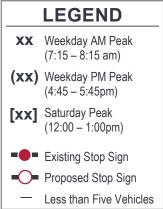
Travaling to From	Estimated Tri	p Distribution
Traveling to/from	Primary Trips	Pass-By Trips ¹
Roadway Direction	%	%
East on IL 64	40%	90%
West on IL 64	40%	10%
North on Fieldgate Drive	20%	-
Total	100%	100%

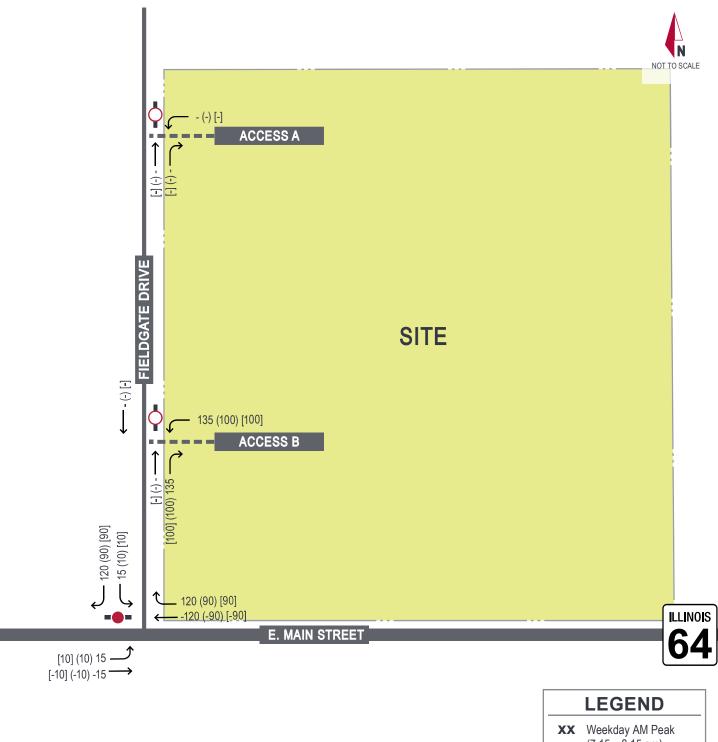
¹Pass-by trips are categorized by the trip's origin.

As noted, Access A is necessary on the site to facilitate fuel truck operations. Fueling occurs from the passenger side of the vehicle. Therefore, the fuel truck would enter at Access A, dispense fuel into the underground storage tanks, and then exit Access B. Fueling operations are expected to occur outside of peak hours and therefore no trips at Access A were included in the study.

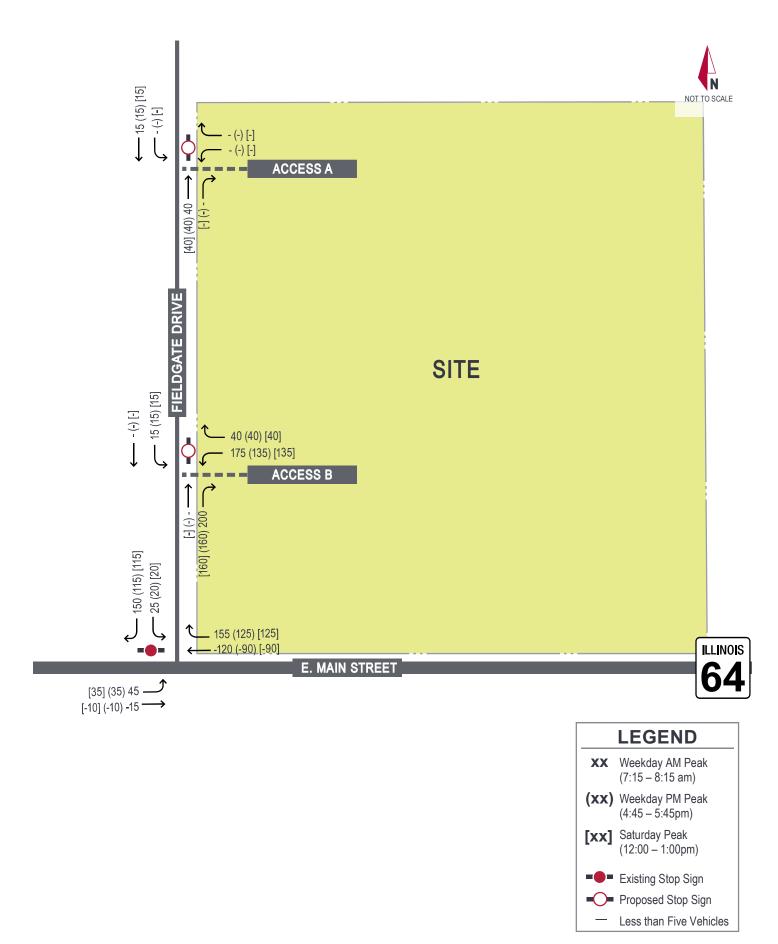
Based on these assumptions, the site trip assignment for primary trips and pass-by trips are illustrated on **Exhibit 3** and **Exhibit 4**, respectively. The total site-generated trips are depicted in **Exhibit 5**.







- (7:15 8:15 am)
- (xx) Weekday PM Peak (4:45 - 5:45pm)
- [xx] Saturday Peak (12:00 1:00pm)
- Existing Stop Sign
- Proposed Stop Sign
 - Less than Five Vehicles





4. FUTURE CONDITIONS

This section of the report outlines the proposed site plan, summarizes site-specific traffic characteristics, and develops future traffic projections for analysis.

Future Background Traffic Projections

Background traffic volumes were estimated using data from the Chicago Metropolitan Agency for Planning (CMAP). Based on information received from CMAP, traffic growth on IL 64 is projected at a compounded rate of roughly 0.64 percent annually through Year 2050. To be conservative for the analysis, the 0.64 percent was applied to Fieldgate Drive to account for background traffic growth. An official letter from CMAP documenting the projected Year 2050 traffic volume on the study roadways is included in the appendix. The future background traffic volumes for Year 2027 are presented in **Exhibit 6**.

Future No-Build Capacity Analysis

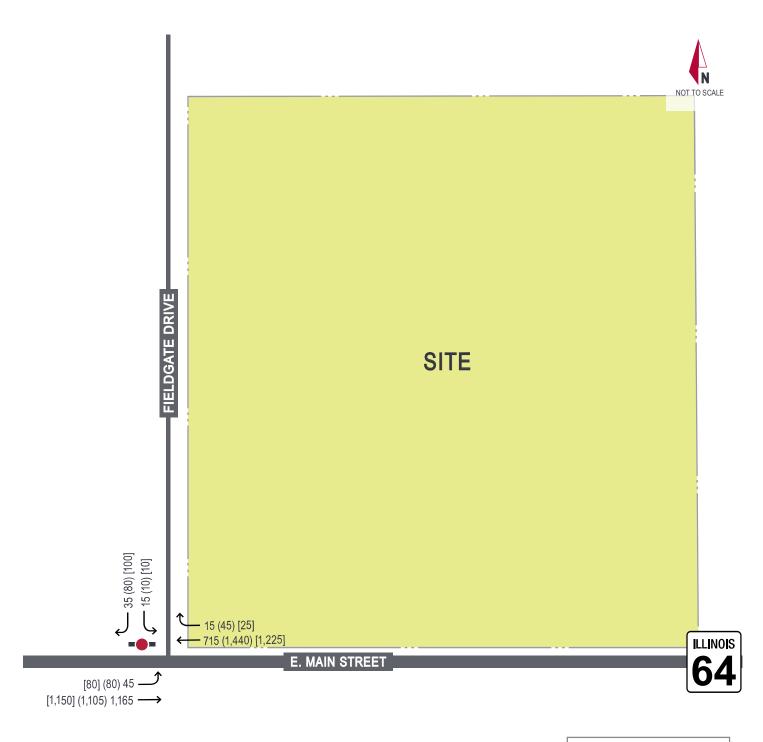
Based on these volume projections, capacity results were identified for the study intersections under future (2027) no-build conditions. The results of capacity analysis are summarized in **Table 4.1** Consistent with the existing conditions analysis, the results are based on Synchro's HCM 6th Edition reports, copies of which are included in the appendix.

Table 4.1 Future No-Build Levels of Service

	Weekday	AM Peak	Weekday P	M Peak	Saturday Midday Peak		
Intersection	Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	
IL 64 / Fieldgate Drive △							
Southbound							
Left-Turn	21	С	44	Е	35	D	
Right-Turn	11	В	19	С	17	С	
Approach	14	В	21	С	18	С	
Eastbound							
Left-Turn	10-	Α	16	С	13	В	

^{△-} Minor-Leg Stop-Controlled Intersection

At the minor-leg stop-controlled intersection of IL 64 and Fieldgate Drive, all approaches are projected to continue to operate acceptably for each of the AM, PM, and Saturday peak hours. Under the Future 2027 No-Build traffic conditions, all approaches are anticipated to remain at the same LOS grades compared to the Existing 2021 traffic conditions. For this study intersection, the 95th percentile queues estimates are approximately one vehicle (approximately 25 feet) or less for all approaches in each peak hour.



LEGEND

- Weekday AM Peak (7:15 8:15am)
- (**xx**) Weekday PM Peak (4:45 5:45pm)
- [**xx**] Saturday Peak (12:00 1:00pm)
- Existing Stop Sign
 - Less than Five Vehicles



Future Geometry

Turn Lane Analysis

Total traffic projections for Year 2027 were calculated by adding the site-generated trips (**Exhibit 5**) to future no-build traffic projections (**Exhibit 6**). Traffic projections for the future (2027) build scenario are illustrated in **Exhibit 7**. For the analysis of future traffic conditions, the existing intersection geometrics and control was assumed as there are no planned improvements in the area. A review of turn lane warrants was completed based on criteria outlined in the IDOT guidelines provided in the IDOT *Bureau of Design and Environment (BDE) Manual.*

For the analysis of future traffic conditions, turn lane warrants were evaluated for the study intersections and the proposed site access driveways using guidelines in the IDOT *BDE Manual*. Based on the IDOT *BDE Manual* volume guidance provided for unsignalized intersections on two-lane facilities, projected future traffic volumes do not meet warrant criteria for a southbound left-turn lane or a northbound right-turn lane on Fieldgate Drive at Access A or a southbound left-turn lane at Access B. A northbound right-turn lane is warranted at Access B based on the *BDE Manual*. Per coordination with the City of St. Charles, Fieldgate Drive should be restriped to provide a northbound right-turn lane as its cross section is wide enough for two (2) lanes. Therefore, a northbound right-turn lane was included in the analysis of future build conditions.

Signal Warrant Analysis

In addition to the turn lane warrants, a signal warrant analysis was performed according to criteria set by the *Manual on Uniform Traffic Control Devices* (MUTCD) for future traffic projections at the intersection of IL 64 and Fieldgate Drive.

A signal warrant analysis was performed according to criteria set for Warrant 1 (Eight-Hour Warrant), Condition A (Minimum Vehicular Volume) and Condition B (Interruption of Continuous Traffic). Warrant 1 can be satisfied by meeting any one of three conditions: Condition A (Minimum Vehicular Volume), Condition B (Interruption of Continuous Traffic), or a combined Condition A & B that has reduced volume thresholds that must be met for both conditions in order to warrant a signal. This warrant is typically evaluated with at least eight hours of traffic count data for an intersection. Because only peak hour projections can be formulated for the proposed development, typical IDOT practice allows a signal warrant to instead be evaluated by reducing peak hour volumes to 55 percent of their projected total to represent the minimum volume during a given eight-hour period. Minor-street right-turning volumes were also reduced at the study intersections in accordance with Pagone's Theorem, per IDOT requirements. These reduced volumes were compared to MUTCD criteria for signal warrant analysis.

Table 4.2 reports the signal warrant analysis conducted for Year 2027 Build traffic conditions.

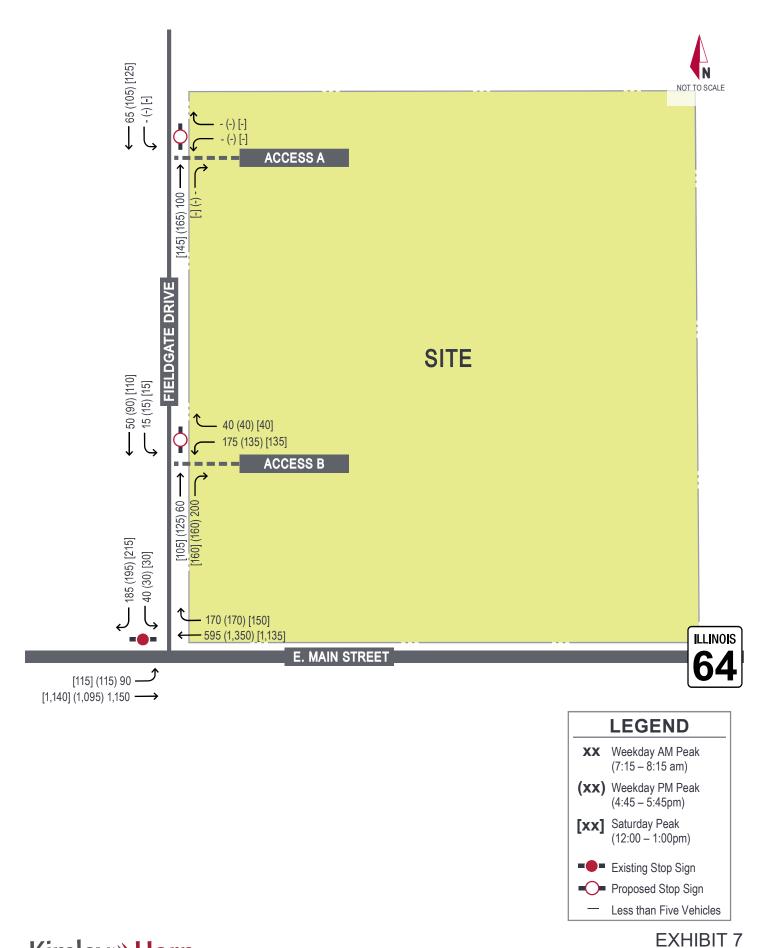




Table 4.2 Summary of Signal Warrant Analyses

Intersection / Scenario	Major Street	Higher-Volume Minor-Leg Approach	Meets Warrant?
MUTCD Criteria for four-lane Major Street w	ith four-lane Minor Street (35	MPH, SRA)	
Warrant 1A	600	200	
Warrant 1B	900	150	
Combination ¹			
Warrant 1A			
Warrant 1B			
IL 64 / Fieldgate Drive	1,502	59	No

¹To satisfy warrant criteria for the combined Conditions A & B, the minimum volume thresholds for both conditions must be met.

As shown in **Table 4.2**, a signal warrant is not met at the study intersection. For the Future (2027) Build traffic conditions, minor-leg stop control is recommended for outbound traffic at each study intersection.

Access A was assumed to provide one inbound lane, one outbound left-turn lane, and one outbound right-turn lane with minor-leg stop-control. Access A is necessary on the site to facilitate fuel truck operations. Fueling occurs from the passenger side of the vehicle. Therefore, the fuel truck would enter at Access A, dispense fuel into the underground storage tanks, and then exit Access B. Fueling operations are expected to occur outside of peak hours and therefore no trips at Access A were included in the study.

Access B was assumed to provide two inbound lanes, one outbound left-turn lane, and one outbound right-turn lane with minor-leg stop-control, the same as existing conditions.



Future Build Capacity Analysis

Based on the volume projections presented in **Exhibit 7**, capacity results were identified for the study intersections under Future Year 2027 Build conditions. The results of capacity analysis are summarized in **Table 4.3**.

Table 4.3 Future Build Level of Service

Intersection		Weekday	AM Peak	Weekday	PM Peak	Saturday Midday Peak		
IIILEI SECTION		Delay (s/veh)	LOS	Delay (s/veh)	LOS	Delay (s/veh)	LOS	
IL 64 / Fieldgate Drive	Δ							
Southbound								
Left-Turn		23	С	>120	F	>120	F	
Right-Turn		13	В	36	D	22	D	
Approach		14	В	89	F	51	F	
Eastbound								
Left-Turn		10-	Α	18	С	14	В	
Fieldgate Drive / Access A	\triangle							
Southbound								
Left-Turn		7	Α	8	А	8	Α	
Westbound								
Left-Turn		9	Α	10+	В	10+	В	
Right-Turn		9	Α	9	Α	9	Α	
Approach		9	Α	10-	Α	10-	Α	
Fieldgate Drive / Access B	Δ							
Southbound								
Left-Turn		8	Α	8	Α	8	Α	
Westbound								
Left-Turn		11	В	11	В	11	В	
Right-Turn		9	Α	9	А	9	Α	
Approach		11	В	12	В	12	В	

^{△ -} Minor-Leg Stop-Controlled Intersection

At the minor-leg stop-controlled intersection of IL 64 and Fieldgate Drive, all approaches are projected to continue to operate acceptably at LOS B or better for the AM peak hour. Under the Future 2027 Build traffic conditions, the southbound approach is anticipated to increase from LOS C to LOS F in the PM and Saturday peak hours compared to the Future Year 2027 No-Build traffic conditions. Low levels-of-service for side-street approaches are not uncommon, as vehicles may experience significant delays turning onto a major roadway. The eastbound left-turn at the study intersection is anticipated to operate similarly to the Future Year 2027 No-Build traffic conditions with no changes to LOS grades in any of the peak hours.

For this study intersection, the 95th percentile queues estimates are 1 vehicle or less (<25 feet) for the eastbound left-turn approach in each peak hour. As noted in the trip generation and distribution sections of this report, traffic volumes at this intersection may be conservatively high, resulting in 95th percentile estimated queues of up to 4 vehicles (100 feet) in the PM peak hour, 3 vehicles (75 feet) in the Saturday peak hour, and 1 vehicle (25 feet) in the AM peak hour at the southbound approach.



Additionally, there are many alternate route opportunities through the connectivity of the site to the surrounding shopping center and to adjacent signalized intersections on Foxfield Road accessible via Fieldgate Drive. This analysis may be conservative since outbound site traffic is likely to make an alternate route choice to avoid visible queues when exiting the site.

At the unsignalized intersections of Fieldgate Drive and Access A and Fieldgate Drive and Access B, all approaches are anticipated to operate at LOS B or better under the Future Year 2027 Build traffic conditions for each peak hour. During each peak hour, the 95th percentile queues estimated at the intersection are less than one vehicle (<25 feet).



5. RECOMMENDATIONS & CONCLUSIONS

Based on Kimley-Horn's review of the proposed site plan and evaluation of existing and future traffic conditions, the study intersections are projected to adequately accommodate the proposed development with the implementation of the following improvements:

Fieldgate Drive / Access A

- Provide a single inbound lane and one outbound left-turn lane and one outbound rightturn lane
- Minor-leg stop control should be posted for outbound traffic

Fieldgate Drive / Access B

- Restripe Fieldgate Drive to provide a dedicated northbound right-turn lane
- Provide two inbound lanes and one outbound left-turn lane and one outbound right-turn lane (existing conditions)
- Minor-leg stop control should be posted for outbound traffic

No improvements are recommended for the existing minor-leg stop-controlled intersection of IL 64 and Fieldgate Drive. The study intersection does not warrant a signal or additional turn-lanes based on the future build traffic conditions presented in this analysis.

Regardless of the final configuration of the intersection geometrics, several additional items should be taken into consideration when preparing site and roadway improvement plans for the subject development. As the site design progresses, care should be taken with landscaping, signage, and monumentation at the site access locations to ensure that adequate horizontal sight distance is provided from the new stop bars. If alterations to the site plan or land use should occur, changes to the analysis provided within this traffic impact study may be needed.



APPENDIX

Conceptual Site Plan

Traffic Count Data

CMAP Year 2050 Projections

Existing (2021) Capacity Reports

Data from the ITE Manual Trip Generation, Tenth Edition

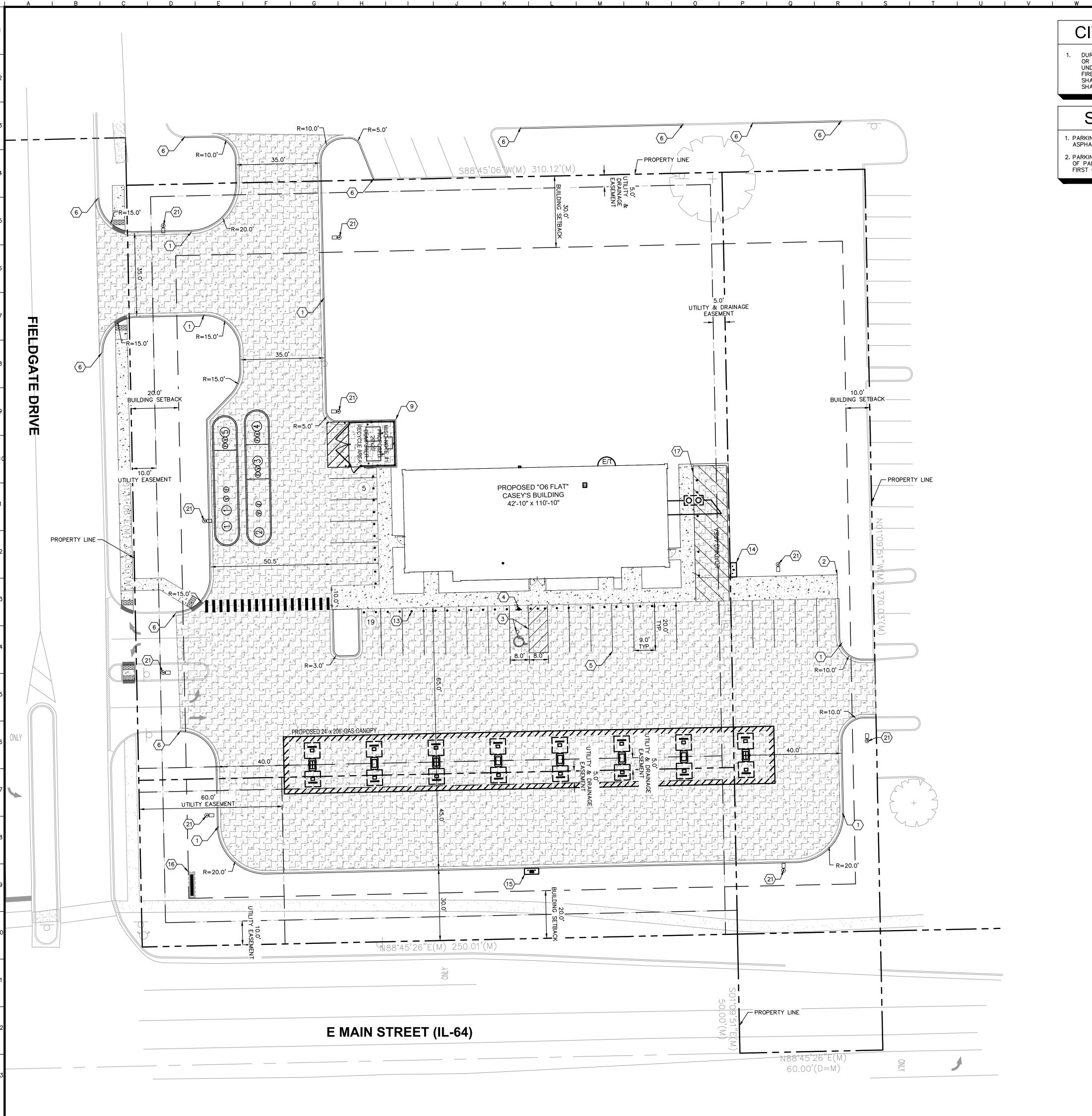
Data from the ITE Trip Generation Handbook, Third Edition

Future (2027) No-Build Capacity Reports

Future (2027) Build Capacity Reports



CONCEPTUAL SITE PLAN



CITY OF ST CHARLES NOTES

DURING CONSTRUCTION, ALL ROADS SHALL BE HARD SURFACED (TEMPORARY OR PERMANENT) AND IN PLACE, CAPABLE OF SUPPORTING VEHICLE LOADING UNDER ALL WEATHER CONDITIONS, PURSUANT TO THE 2015 INTERNATIONAL FIRE CODE, CHAPTER 5, CHAPTER 33, AND APPENDIX D. THE ADDITIONAL OF SHALL BE AN ACCEPTABLE MATERIAL. ACCESS FOR FIRE DEPARTMENT VEHICLES SHALL BE MAINTAINED AT ALL TIMES.



STRIPING REQUIREMENTS

. PARKING LOT STRIPING SHALL NOT BE APPLIED WITHIN 24 HOURS OF ASPHALT INSTALLATION.

2. PARKING LOT STRIPING SHALL BE TWO COATS OF PAINT. SECOND COAT OF PAINT SHALL BE APPLIED A MINIMUM OF 24 HOURS AFTER THE

KEY NOTES

- 1 B6.12 CONCRETE CURB AND GUTTER, TYP. (SEE DETAILS)
- 2 CONCRETE SIDEWALK, TYP. (SEE DETAILS)
- 3 ACCESSIBLE PAVEMENT MARKINGS, TYP. (SEE DETAILS)
- 4 ACCESSIBLE PARKING SIGN, TYP. (MUTCD R7-8, SEE DETAILS)
- 5 4" WIDE PAINTED SOLID LINE, TYP.
- (6) CONNECT TO EXISTING PAVEMENT, SIDEWALK, CURB, TYP.
- $\langle 7 \rangle$ 24" WIDE STOP BAR, TYP. (SEE DETAILS)
- 8 STOP SIGN, TYP. (MUTCD R1-1, SEE DETAILS)
- (9) TRASH ENCLOSURE (SEE ARCHITECTURAL PLANS FOR DETAILS) (10) DEPRESSED CURB AND GUTTER
- (11) ACCESSIBLE RAMP (SEE DETAILS)
- (12) DETECTABLE WARNINGS
- (13) BOLLARD, TYP. (SEE DETAILS)
- (14) AIR COMPRESSOR BOX
- (15) EMERGENCY SHUT-OFF SWITCH
- (16) MONUMENT OR PYLON SIGN (SEE ARCHITECTURAL PLANS FOR DETAILS)
- (17) PAVEMENT STRIPING
- (18) RIGHT IN ONLY SIGN, TYP. (MUTCD R1-1, SEE DETAILS)
- (19) DO NOT ENTER SIGN
- (20) APPROXIMATE LOCATION OF SOIL BORING (SEE GEOTECHNICAL REPORT FOR DETAILS)
- (21) LIGHT POLE (SEE PHOTOMETRIC PLAN FOR DETAILS)

PAVING AND CURB LEGEND



CONCRETE SIDEWALK
SEE CONSTRUCTION DETAILS FOR PAVEMENT SECTION

NEW CONSTRUCTION OF CASEYS FUEL CENTER

SECTION 25, TOWNSHIP 40N, RANGE 8E

CONCRETE PAVEMENT
SEE CONSTRUCTION DETAILS FOR PAVEMENT SECTION

STANDARD PITCH CONCRETE CURB AND GUTTER REVERSE PITCH CONCRETE CURB AND GUTTER CONCRETE DEPRESSED CURB AND GUTTER

2600 E. MAIN ST.

EAST: BC PUD WEST: BC PUD

ST. CHARLES, IL 60172

NORTH: BC PUD SOUTH: BC PUD & BC

N/A 2.35 AC (102,226 SF)

COMMUNITY BUSINESS (BC) PUD COMMERCIAL — OFFICE

COMMERCIAL - FUEL STATION



PROJECT DESCRIPTION: LOCATION: ADDRESS:

PLANNING DISTRICT: **EXISTING LAND USE:** PROPOSED LAND USE: SURROUNDING LAND USE:

FLOOD ZONE: SITE AREA: NET DEVELOPED AREA: MAX BUILDING HEIGHT: FLOOR AREA RATIO:

LOT COVERAGE: BUILDING AREA: IMPERVIOUS AREA: PERVIOUS AREA:

BUILDING SETBACKS:

LANDSCAPE BUFFERS (PER PUD):

52,400 SF 46,855 SF FRONT: 30 FT, INTERIOR SIDE: 15 FT, EXTERIOR SIDE: 32 FT, REAR: 100 FT

4,747 SF

2.35 AC

21 FT

0.046

PARKING REQUIREMENTS:
STANDARD PARKING SPACES PROVIDED: 23 SPACES ACCESSIBLE PARKING SPACES REQUIRED: 1 SPACE ACCESSIBLE PARKING SPACES PROVIDED: 1 SPACE

TOTAL PARKING SPACES PROVIDED: 24 SPACES

Kimley » Horn

SASEY'S SCHARLE

ORIGINAL ISSUE: 07/09/2021 KHA PROJECT NO. 168865004

SHEET NUMBER

C-101



TRAFFIC COUNT DATA

Report Summary

			So	uthbou	ınd			W	estbou	nd			Ea	astbour	nd					Crosswalk	
Time Period	Class.	R	L	U	- 1	0	R	Т	U	- 1	0	T	L	U	1	0	Total		Bicycles	Pedestrians	Total
AM Peak Hour	Lights	31	16	0	47	61	15	642	0	657	1057	1041	46	0	1087	673	1791	Ν	1	0	1
Specified Period	%	94%	100%	0%	96%	95%	88%	93%	0%	93%	93%	93%	98%	0%	93%	93%	93%		100%	0%	
7:15 AM - 8:15 AM	Mediums	2	0	0	2	3	2	26	0	28	44	44	1	0	45	28	75	Ε	0	0	0
One Hour Peak	%	6%	0%	0%	4%	5%	12%	4%	0%	4%	4%	4%	2%	0%	4%	4%	4%		0%	0%	
7:15 AM - 8:15 AM	Articulated Trucks	0	0	0	0	0	0	21	0	21	33	33	0	0	33	21	54	W	0	0	0
	%	0%	0%	0%	0%	0%	0%	3%	0%	3%	3%	3%	0%	0%	3%	3%	3%		0%	0%	
	Total	33	16	0	49	64	17	689	0	706	1134	1118	47	0	1165	722	1920		1	0	1
	PHF	0.82	0.67	0	0.82	0.84	0.71	0.86	0	0.86	0.9	0.89	0.84	0	0.9	0.86	0.95				
	HV %	6%	0%	0%	4%	5%	12%	7%	0%	7%	7%	7%	2%	0%	7%	7%	7%				
PM Peak Hour	Lights	75	10	0	85	116	46	1369	0	1415	1045	1035	70	1	1106	1445	2606	N	0	0	0
Specified Period	%	100%	100%	0%	100%	98%	100%	99%	0%	99%	97%	97%	97%	100%	97%	99%	98%		0%	0%	
4:45 PM - 5:45 PM	Mediums	0	0	0	0	2	0	5	0	5	19	19	2	0	21	5	26	Ε	0	0	0
One Hour Peak	%	0%	0%	0%	0%	2%	0%	0%	0%	0%	2%	2%	3%	0%	2%	0%	1%		0%	0%	
4:45 PM - 5:45 PM	Articulated Trucks	0	0	0	0	0	0	11	0	11	9	9	0	0	9	11	20	W	0	0	0
	%	0%	0%	0%	0%	0%	0%	1%	0%	1%	1%	1%	0%	0%	1%	1%	1%		0%	0%	
	Total	75	10	0	85	118	46	1385	0	1431	1073	1063	72	1	1136	1461	2652		0	0	0
	PHF	0.72	0.62	0	0.76	0.76	0.64	0.96	0	0.95	0.94	0.93	0.72	0.25	0.92	0.96	0.96				
	HV %	0%	0%	0%	0%	2%	0%	1%	0%	1%	3%	3%	3%	0%	3%	1%	2%				

Study Name 01 East Main Street & Fieldgate Drive Start Date Saturday, March 27, 2021

Report Summary

			Soi	uthbou	ınd			Westbound Eastbound											Crosswalk		
Time Period	Class.	R	L	U	l l	0	R	Т	U		0	T	L	U	I	0	Total		Bicycles	Pedestrians	Total
Saturday Peak Period	Lights	93	10	0	103	99	25	1171	0	1196	1100	1090	74	0	1164	1264	2463	N	0	0	0
Specified Period	%	96%	100%	0%	96%	100%	100%	99%	0%	99%	99%	99%	100%	0%	99%	99%	99%		0%	0%	
12:00 PM - 1:00 PM	Mediums	4	0	0	4	0	0	8	0	8	7	7	0	0	7	12	19	Ε	0	0	0
One Hour Peak	%	4%	0%	0%	4%	0%	0%	1%	0%	1%	1%	1%	0%	0%	1%	1%	1%		0%	0%	
12:00 PM - 1:00 PM	Articulated Trucks	0	0	0	0	0	0	3	0	3	7	7	0	0	7	3	10	W	0	0	0
	%	0%	0%	0%	0%	0%	0%	0%	0%	0%	1%	1%	0%	0%	1%	0%	0%		0%	0%	
	Total	97	10	0	107	99	25	1182	0	1207	1114	1104	74	0	1178	1279	2492		0	0	0
	PHF	0.9	0.83	0	0.92	0.73	0.89	0.89	0	0.9	0.94	0.94	0.69	0	0.92	0.89	0.93				
	HV %	4%	0%	0%	4%	0%	0%	1%	0%	1%	1%	1%	0%	0%	1%	1%	1%				



CMAP YEAR 2050 PROJECTIONS

TRAFFIC FORECAST RECORD

Record Number: ka-10-21

Type of Report: Projection

Year Sought: 2050

Analyst: JAR

Organization requesting forecast: Kimley-Horn

Contact: Danielle Kronowski, EIT

Email or Phone danielle.kronowski@kimley-horn.com

Sponsor: IDOT

Date request was received: March 31, 2021

Date that response was emailed: March 31, 2021

Facility Location: IL 64 from Fieldgate Drive to Kirk Rd

Municipality: St. Cjharles



433 West Van Buren Street Suite 450 Chicago, IL 60607

> 312-454-0400 cmap.illinois.gov

March 31, 2021

Danielle Kronowski, EIT Transportation Analyst Kimley-Horn 1001 Warrenville Road Suite 350 Lisle, IL 60532

Subject: IL 64 from Fieldgate Drive to Kirk Road

IDOT

Dear Ms. Kronowski:

In response to a request made on your behalf and dated March 31, 2021, we have developed year 2050 average daily traffic (ADT) projections for the subject location.

ROAD SEGMENT	Current Volume	Year 2050 ADT
IL 64 (E. Main St) from Fieldgate Dr to Kirk Rd	29,500	36,000

Traffic projections are developed using existing ADT data provided in the request letter and the results from the June 2020 CMAP Travel Demand Analysis. The regional travel model uses CMAP 2050 socioeconomic projections and assumes the implementation of the ON TO 2050 Comprehensive Regional Plan for the Northeastern Illinois area. The provision of this data in support of your request does not constitute a CMAP endorsement of the proposed development or any subsequent developments.

If you have any questions, please call me at (312) 386-8806.

Sincerely,

Jose Rodriguez, PTP, AICP

Senior Planner, Research & Analysis

cc: Quigley (IDOT)

2021_CY_TrafficForecast\St.Charles\ka-10-21\ka-10-21.docx



EXISTING (2021) CAPACITY REPORTS

Weekday Morning Peak Hour

Weekday Evening Peak Hour

Saturday Midday Peak Hour

Intersection							
Int Delay, s/veh	0.6						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	CDL Š			VVDR	SDL 1	JDK ř	
Traffic Vol, veh/h	1 45	↑ ↑	↑↑ 690	r 15	1 5	35	
Future Vol, veh/h	45	1120	690	15	15	35	
Conflicting Peds, #/hr	40	0	090	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	riee -	None	riee -		Stop -	None	
Storage Length	120	NOITE	_	140	0	0	
Veh in Median Storage		0	0	-	0	-	
Grade, %	·, +- -	0	0	<u>-</u>	0	_	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	7	7	12	2	6	
Mvmt Flow	47	1179	726	16	16	37	
IVIVIII I IOVV	71	1113	120	10	10	01	
	Major1		Major2		Minor2		
Conflicting Flow All	742	0	-	0	1410	363	
Stage 1	-	-	-	-	726	-	
Stage 2	-	-	-	-	684	-	
Critical Hdwy	4.14	-	-	-	6.84	7.02	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	-	-	-	-	5.84	-	
Follow-up Hdwy	2.22	-	-	-	3.52	3.36	
Pot Cap-1 Maneuver	861	-	-	-	129	622	
Stage 1	-	-	-	-	440	-	
Stage 2	-	-	-	-	462	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	861	-	-	-	122	622	
Mov Cap-2 Maneuver	-	-	-	-	255	-	
Stage 1	-	-	-	-	416	-	
Stage 2	-	-	-	-	462	-	
Annroach	EB		MD		CD		
Approach			WB		SB		
HCM Control Delay, s	0.4		0		13.8		
HCM LOS					В		
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR :	SBLn1 S	SBLn2
Capacity (veh/h)		861	_	-	-	255	622
HCM Lane V/C Ratio		0.055	-	_	-	0.062	
HCM Control Delay (s)		9.4	-	-	-	20	11.2
HCM Lane LOS		Α	-	-	-	С	В
HCM 95th %tile Q(veh))	0.2	-	-	-	0.2	0.2

Intersection							
Int Delay, s/veh	1.1						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	CDL Š	↑ ↑	<u>₩</u>	WDK 7	SDL Š	SDR 7	
Traffic Vol, veh/h	75	TT 1065	TT	45	10	75	
Future Vol, veh/h	75	1065	1385	45	10	75	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-		-	None	
Storage Length	120	-	-	140	0	0	
Veh in Median Storage,	# -	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	3	3	2	2	2	2	
Mvmt Flow	79	1121	1458	47	11	79	
Major/Minor M	lajor1	N	Major2	ı	Minor2		
	1505	0	-	0	2177	729	
Stage 1	-	-	_	-	1458	-	
Stage 2	-	-	-	-	719	-	
Critical Hdwy	4.16	-	_	-	6.84	6.94	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	-	-	-	-	5.84	-	
Follow-up Hdwy	2.23	-	-	-	3.52	3.32	
Pot Cap-1 Maneuver	436	-	-	-	39	365	
Stage 1	-	-	-	-	180	-	
Stage 2	-	-	-	-	444	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	436	-	-	-	32	365	
Mov Cap-2 Maneuver	-	-	-	-	111	-	
Stage 1	-	-	-	-	147	-	
Stage 2	-	-	-	-	444	-	
Approach	EB		WB		SB		
HCM Control Delay, s	1		0		20.3		
HCM LOS					С		
Minor Lane/Major Mvmt		EBL	EBT	WBT	WRR :	SBLn1 SI	Bl n2
Capacity (veh/h)		436		-	- 1001		365
HCM Lane V/C Ratio		0.181		_		0.095	
HCM Control Delay (s)		15.1	_	_	_		17.6
HCM Lane LOS		C	_	_	_	+0.0 E	C
HCM 95th %tile Q(veh)		0.7	_	_	_	0.3	0.8
		J.1				0.0	0.0

Intersection							
Int Delay, s/veh	1.1						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	ኘ	^	^	7	ኘ	7	
Traffic Vol, veh/h	75	1105	1180	25	10	95	
Future Vol, veh/h	75	1105	1180	25	10	95	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	_		-	None	
Storage Length	120	-	-	140	0	0	
Veh in Median Storage		0	0	-	0	-	
Grade, %	, -	0	0	-	0	-	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	2	2	2	2	4	
Mvmt Flow	79	1163	1242	26	11	100	
NA ' 184'							
	Major1		Major2		Minor2		
Conflicting Flow All	1268	0	-	0	1982	621	
Stage 1	-	-	-	-	1242	-	
Stage 2	-	-	-	-	740	-	
Critical Hdwy	4.14	-	-	-	6.84	6.98	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	-	-	-	-	5.84	-	
Follow-up Hdwy	2.22	-	-	-	3.52	3.34	
Pot Cap-1 Maneuver	544	-	-	-	54	425	
Stage 1	-	-	-	-	236	-	
Stage 2	-	_	-	_	433	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	544	-	-	-	46	425	
Mov Cap-2 Maneuver	-	-	-	-	143	-	
Stage 1	-	-	-	_	202	-	
Stage 2	-	-	-	-	433	-	
A I			1675		0.5		
Approach	EB		WB		SB		
HCM Control Delay, s	0.8		0		17.6		
HCM LOS					С		
Minor Lane/Major Mvm	t	EBL	EBT	WBT	WRR	SBLn1	SRLn2
		544		VVDI		143	425
Capacity (veh/h)			-	-	-		
HCM Control Polov (a)		0.145	-	-		0.074	
HCM Control Delay (s)		12.7	-	-	-	32.2	16.1
HCM Lane LOS		В	-	-	-	D	С
HCM 95th %tile Q(veh)		0.5	-	-	-	0.2	0.9



DATA FROM THE ITE MANUAL TRIP GENERATION, TENTH EDITION

Land Use: 960 Super Convenience Market/Gas Station

Description

This land use includes gasoline/service stations with convenience markets where there is significant business related to the sale of convenience items and the fueling of motor vehicles. Some commonly sold convenience items include newspapers, freshly brewed coffee, daily-made donuts, bakery items, hot and cold beverages, breakfast items, dairy items, fresh fruits, soups, light meals, ready-to-go and freshly made sandwiches and wraps, and ready-to-go salads. Stores typically also had automated teller machines (ATMs), and public restrooms. The sites included in this land use category have the following two specific characteristics:

- The gross floor area of the convenience market is at least 3,000 gross square feet
- The number of vehicle fueling positions is at least 10

Convenience market with gasoline pumps (Land Use 853) and gasoline/service station with convenience market (Land Use 945) are related uses.

Additional Data

To reflect changing characteristics of the convenience market component of this land use, only data from the past two decades have been included in this land use.

The independent variable, vehicle fueling positions, is defined as the maximum number of vehicles that can be fueled simultaneously. Gasoline/service stations in this land use include "pay-at-the-pump" and traditional fueling stations.

A multi-variable regression analysis based on both the convenience market gross floor area (GFA) and the number of vehicle fueling positions (VFP) produced a series of fitted curve equations. The equations are in the form of:

Vehicle Trips = [(VFP Factor) x (Number of VFP)] + [(GFA Factor) x (GFA)] + (Constant)

The values for the VFP factor, GFA factor, and constant are presented in the following table for each time period for which a fitted curve equation could produce an R² value of at least 0.50.

Time Period	VFP Factor	GFA Factor	Constant	R²
Weekday, AM Peak Hour of Generator	10.3	105	-290	0.62
Weekday, PM Peak Hour of Generator	6.91	76.0	-133	0.68
Weekday, AM Peak Hour of Adjacent Street	16.1	135	-483	0.66
Weekday, PM Peak Hour of Adjacent Street	11.5	82.9	-226	0.51

The sites were surveyed in the late 1990's, 2000s and the 2010s in Florida, Iowa, Maryland, Minnesota, New Hampshire, New Jersey, Pennsylvania, Texas, Utah, and Wisconsin.

Source Numbers

617, 813, 844, 850, 864, 865, 867, 869, 882, 888, 904, 938, 954, 960, 962



(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday

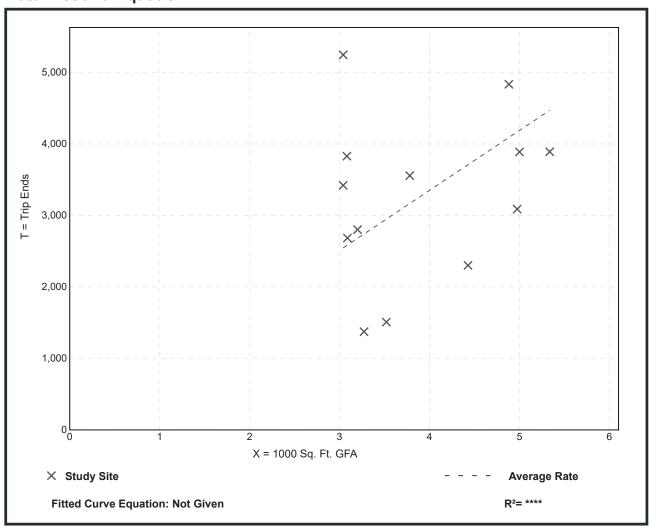
Setting/Location: General Urban/Suburban

Number of Studies: 13 1000 Sq. Ft. GFA: 4

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
837.58	419.93 - 1725.33	334.67





(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

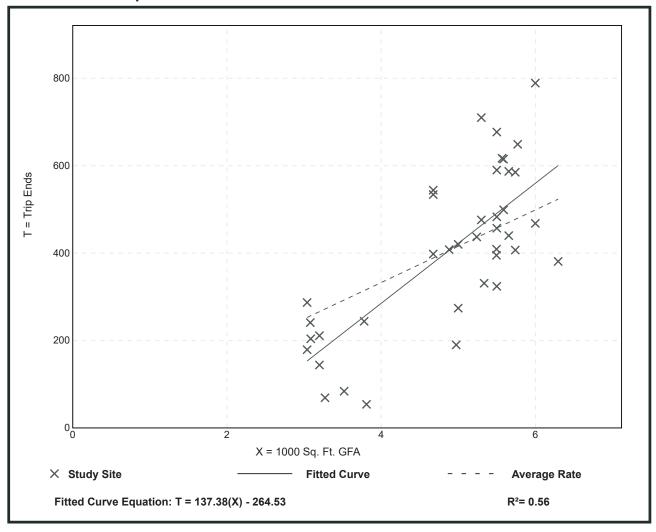
Setting/Location: General Urban/Suburban

Number of Studies: 39 1000 Sq. Ft. GFA: 5

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
83.14	14.17 - 133.96	28.07





(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

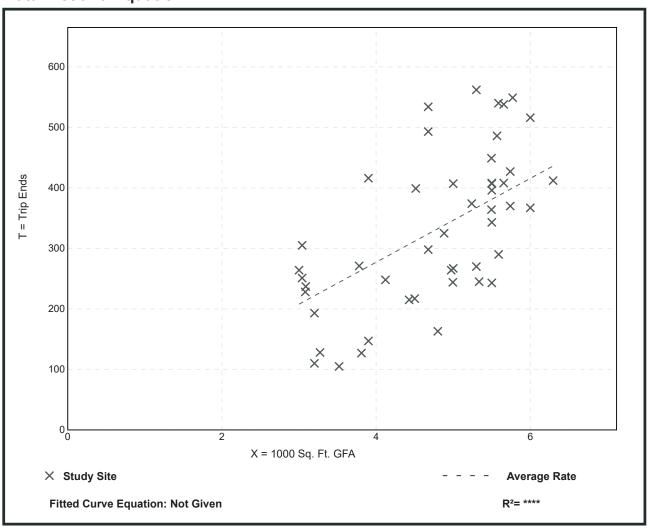
Setting/Location: General Urban/Suburban

Number of Studies: 48 1000 Sq. Ft. GFA: 5

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
69.28	29.83 - 114.20	21.07





(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

AM Peak Hour of Generator

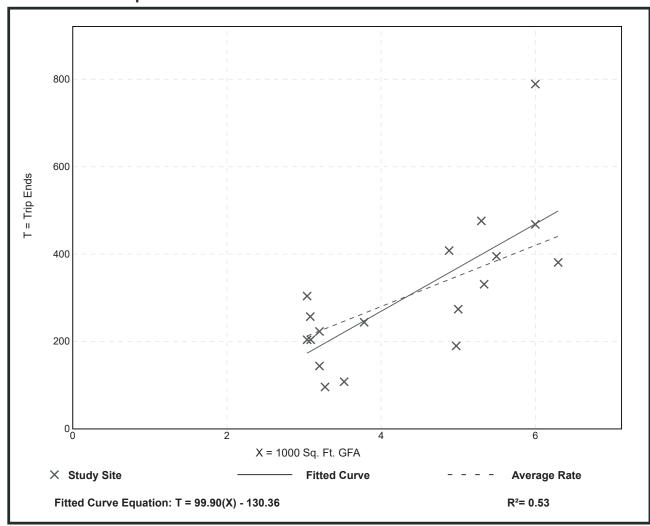
Setting/Location: General Urban/Suburban

Number of Studies: 18 1000 Sq. Ft. GFA: 4

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
70.01	29.34 - 131.50	25.84





(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

PM Peak Hour of Generator

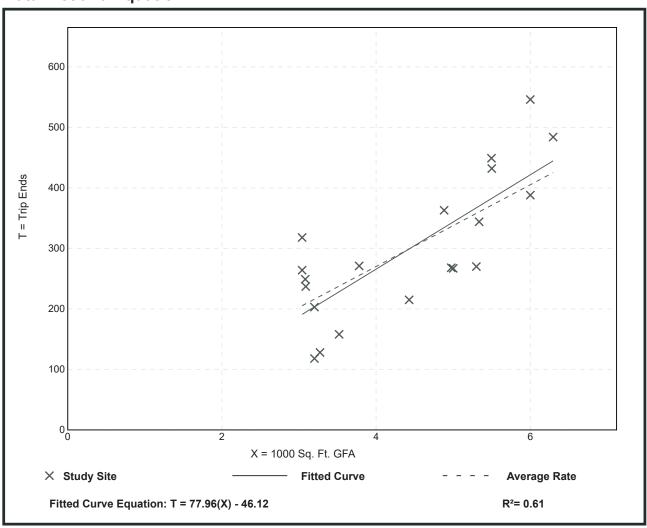
Setting/Location: General Urban/Suburban

Number of Studies: 20 1000 Sq. Ft. GFA: 4

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
67.53	36.88 - 104.61	17.12





(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Saturday

Setting/Location: General Urban/Suburban

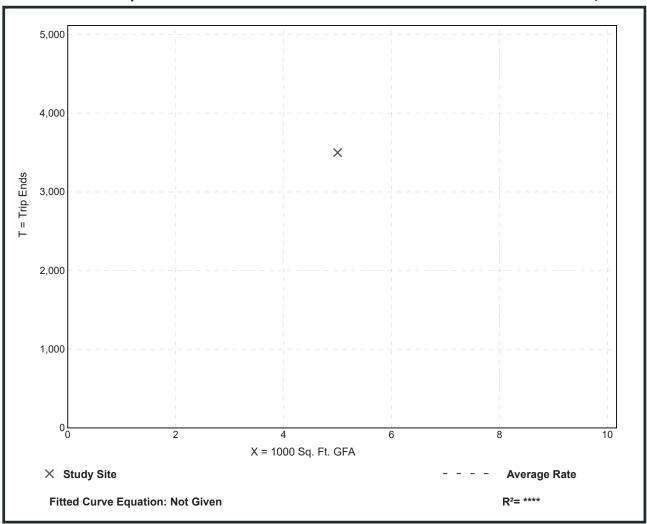
Number of Studies: 1 1000 Sq. Ft. GFA: 5

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
700.00	700.00 - 700.00	*

Data Plot and Equation





(960)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Saturday, Peak Hour of Generator

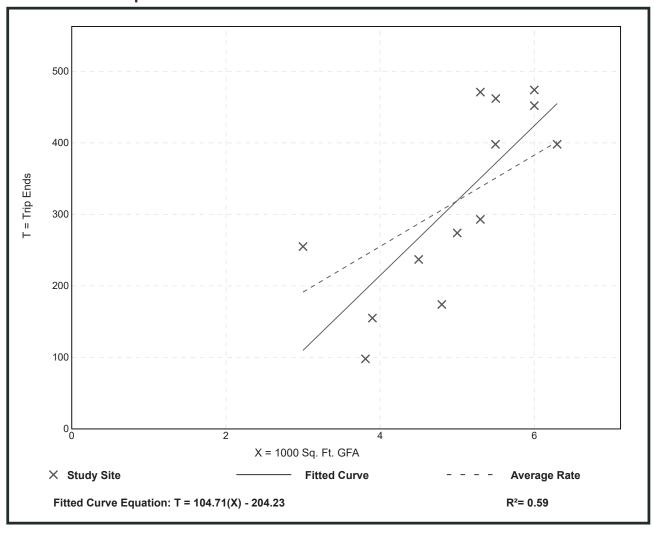
Setting/Location: General Urban/Suburban

Number of Studies: 13 1000 Sq. Ft. GFA: 5

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
63.80	25.72 - 88.87	19.29





(960)

Vehicle Trip Ends vs: AM Peak Hour Traffic on Adj. St.

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

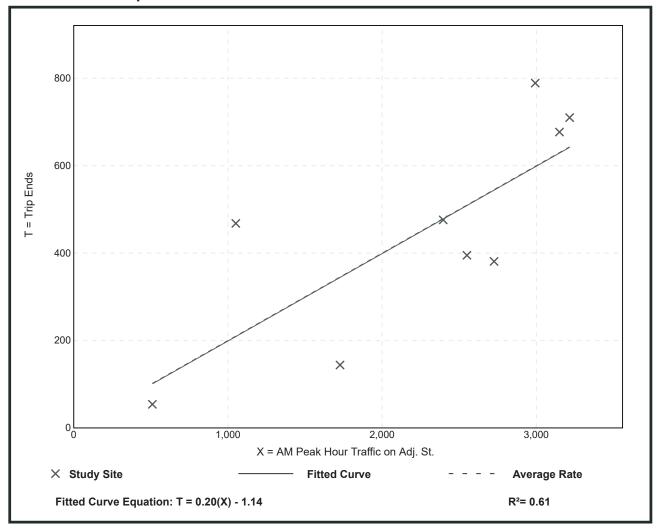
Setting/Location: General Urban/Suburban

Number of Studies: 9 AM Peak Hour Traffic on Adj. St.: 2258

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per AM Peak Hour Traffic on Adj. St.

Average Rate	Range of Rates	Standard Deviation
0.20	0.08 - 0.45	0.08





(960)

Vehicle Trip Ends vs: AM Peak Hour Traffic on Adj. St.

On a: Weekday,

AM Peak Hour of Generator

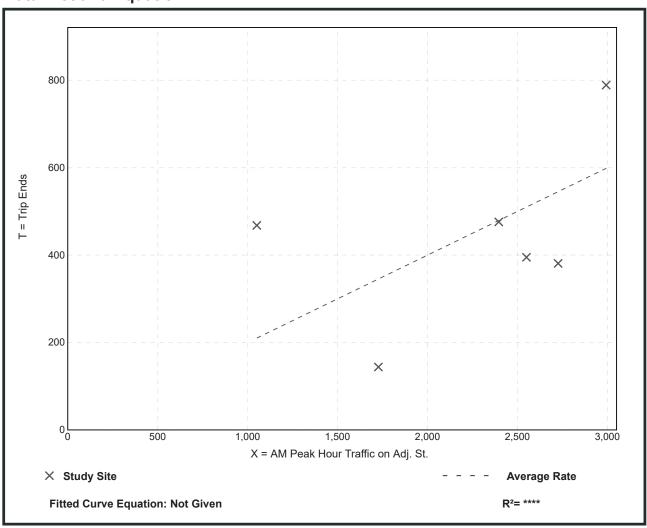
Setting/Location: General Urban/Suburban

Number of Studies: 6 our Traffic on Adj. St.: 2241

AM Peak Hour Traffic on Adj. St.: 2241
Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per AM Peak Hour Traffic on Adj. St.

Average Rate	Range of Rates	Standard Deviation
0.20	0.08 - 0.45	0.10





(960)

Vehicle Trip Ends vs: PM Peak Hour Traffic on Adj. St.

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

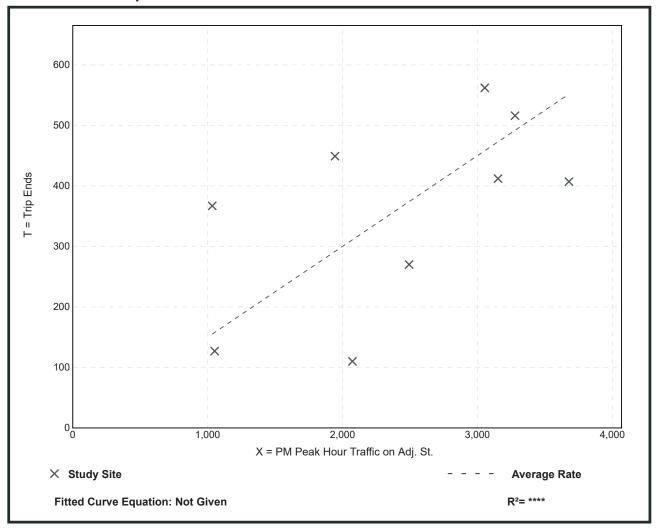
Setting/Location: General Urban/Suburban

Number of Studies: 9
PM Peak Hour Traffic on Adj. St.: 2418

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per PM Peak Hour Traffic on Adj. St.

Average Rate	Range of Rates	Standard Deviation
0.15	0.05 - 0.35	0.07





(960)

Vehicle Trip Ends vs: PM Peak Hour Traffic on Adj. St.

On a: Weekday,

PM Peak Hour of Generator

Setting/Location: General Urban/Suburban

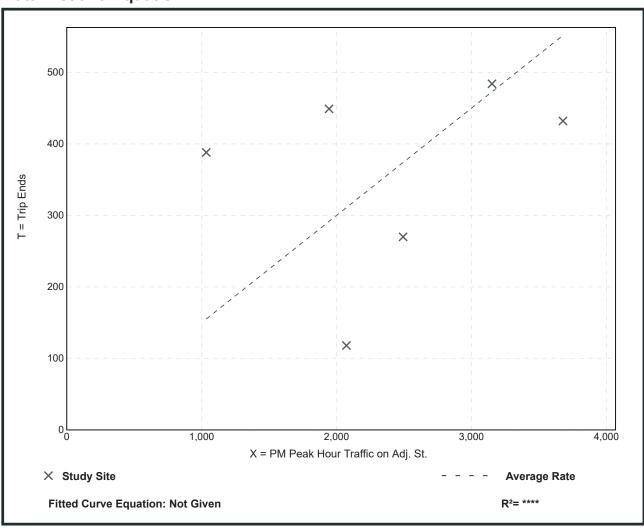
Number of Studies: 6

PM Peak Hour Traffic on Adj. St.: 2396

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per PM Peak Hour Traffic on Adj. St.

Average Rate	Range of Rates	Standard Deviation
0.15	0.06 - 0.38	0.09





(960)

Vehicle Trip Ends vs: Employees

On a: Weekday

Setting/Location: General Urban/Suburban

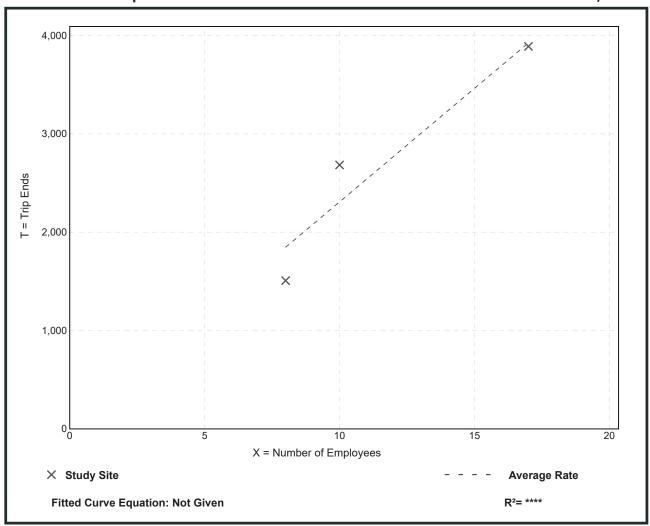
Number of Studies: 3
Avg. Num. of Employees: 12

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Employee

Average Rate	Range of Rates	Standard Deviation
230.91	188.50 - 268.40	34.96

Data Plot and Equation





(960)

Vehicle Trip Ends vs: Employees

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

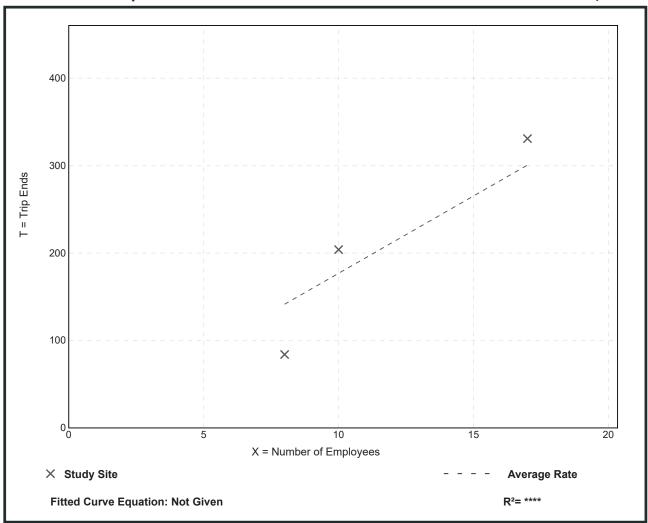
Number of Studies: 3
Avg. Num. of Employees: 12

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Employee

А	verage Rate	Range of Rates	Standard Deviation
	17.69	10.50 - 20.40	4.81

Data Plot and Equation





(960)

Vehicle Trip Ends vs: Employees

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

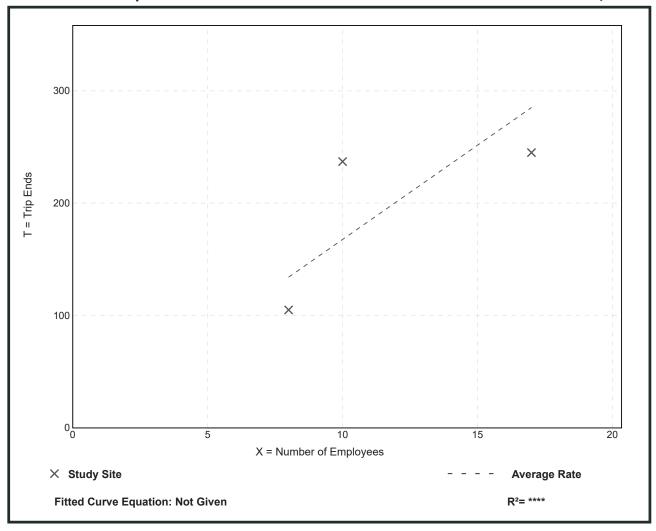
Number of Studies: 3
Avg. Num. of Employees: 12

Directional Distribution: 49% entering, 51% exiting

Vehicle Trip Generation per Employee

Average Rate	Range of Rates	Standard Deviation
16.77	13.13 - 23.70	5.40

Data Plot and Equation





(960)

Vehicle Trip Ends vs: Employees

On a: Weekday,

AM Peak Hour of Generator

Setting/Location: General Urban/Suburban

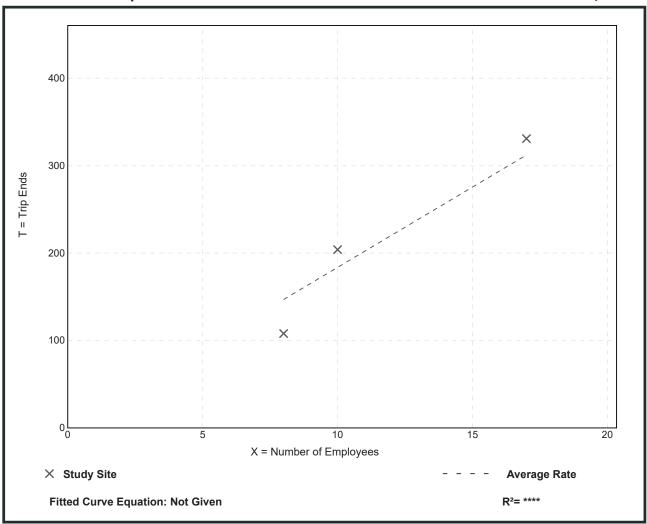
Number of Studies: 3
Avg. Num. of Employees: 12

Directional Distribution: 51% entering, 49% exiting

Vehicle Trip Generation per Employee

Average Rate	Range of Rates	Standard Deviation
18.37	13.50 - 20.40	3.28

Data Plot and Equation





(960)

Vehicle Trip Ends vs: Employees

On a: Weekday,

PM Peak Hour of Generator

Setting/Location: General Urban/Suburban

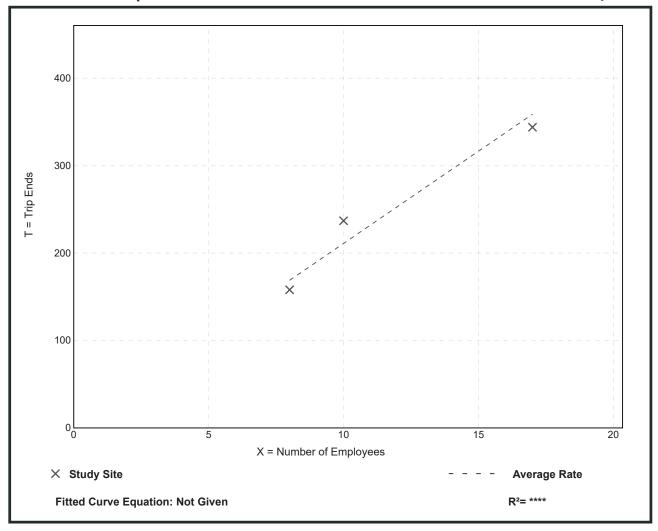
Number of Studies: 3
Avg. Num. of Employees: 12

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Employee

Average Rate	Range of Rates	Standard Deviation
21.11	19.75 - 23.70	2.02

Data Plot and Equation





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday

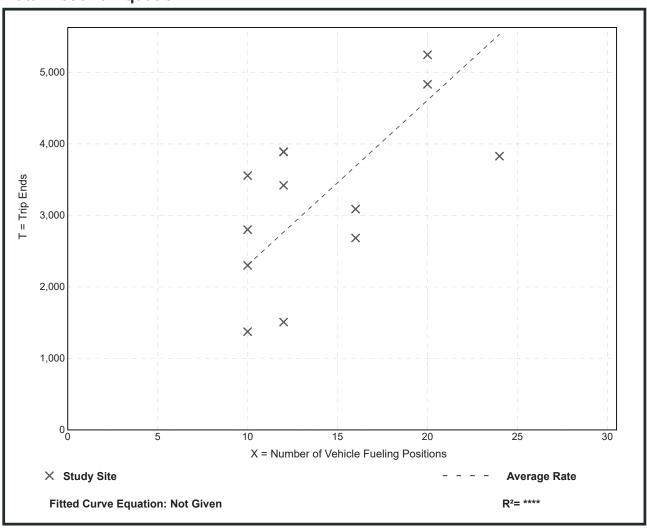
Setting/Location: General Urban/Suburban

Number of Studies: 13 Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
230.52	125.67 - 355.60	71.75





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

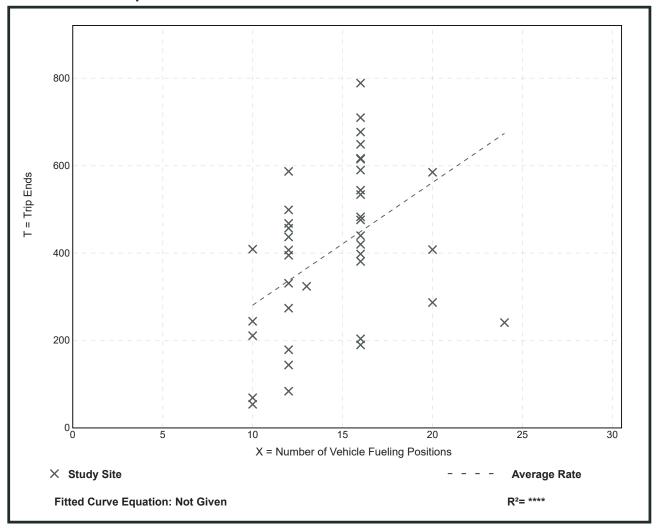
Number of Studies: 39

Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
28.08	5.40 - 49.31	11.98





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday,

Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

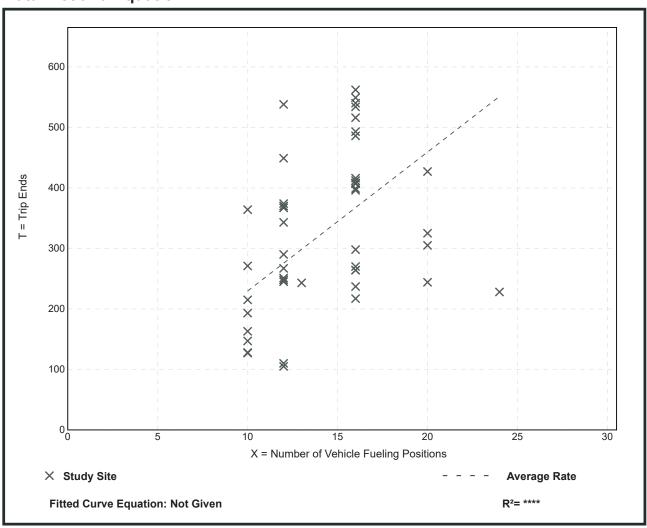
Number of Studies: 48

Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
22.96	8.75 - 44.83	8.34





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday,

AM Peak Hour of Generator

Setting/Location: General Urban/Suburban

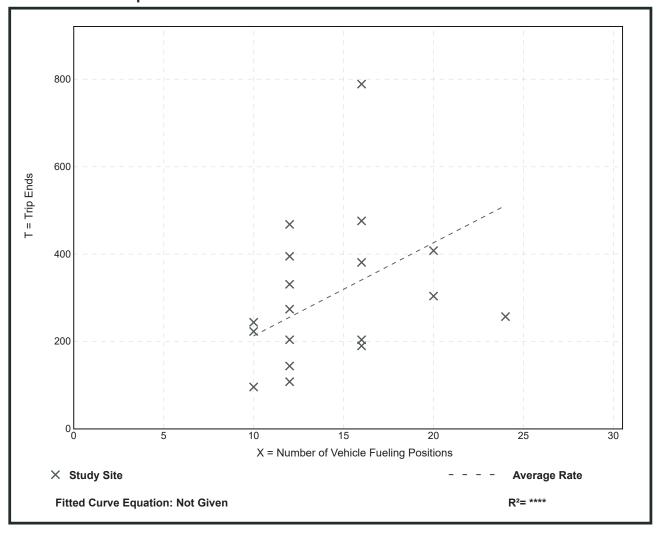
Number of Studies: 18

Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
21.30	9.00 - 49.31	11.15





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Weekday,

PM Peak Hour of Generator

Setting/Location: General Urban/Suburban

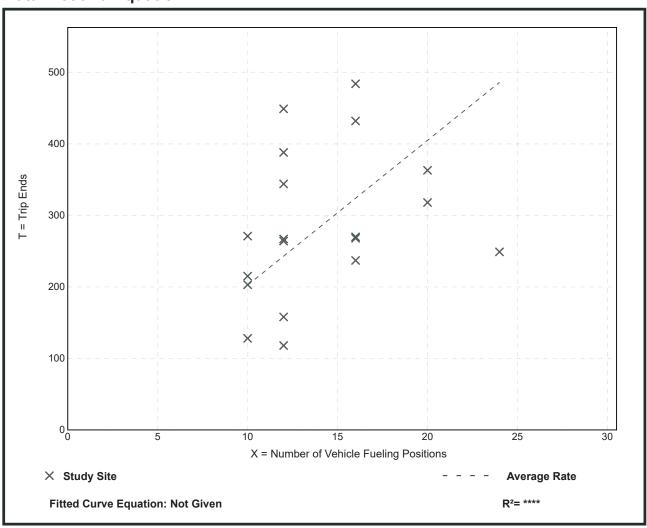
Number of Studies: 19

Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
20.25	9.83 - 37.42	7.73





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Saturday

Setting/Location: General Urban/Suburban

Number of Studies: 1

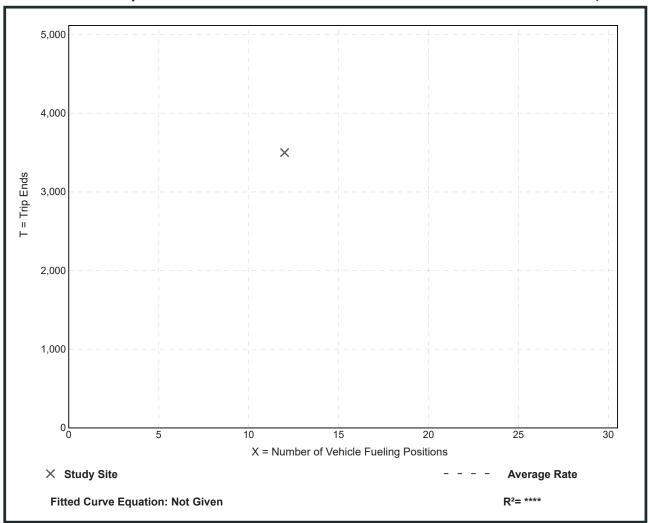
Avg. Num. of Vehicle Fueling Positions: 12

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
291.67	291.67 - 291.67	*

Data Plot and Equation





(960)

Vehicle Trip Ends vs: Vehicle Fueling Positions

On a: Saturday, Peak Hour of Generator

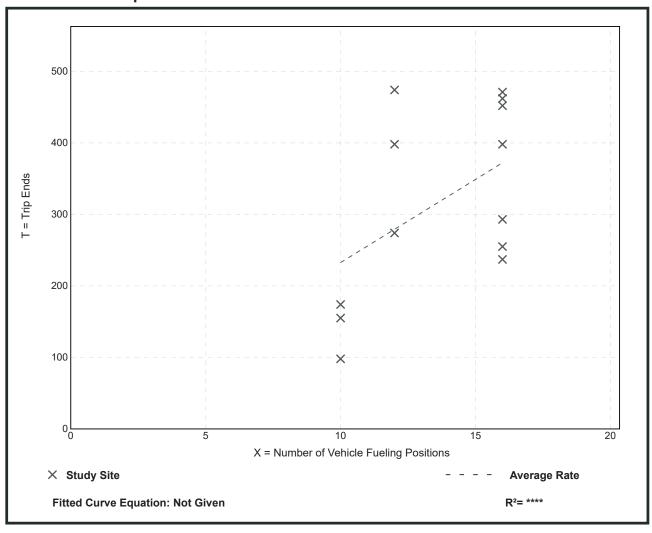
Setting/Location: General Urban/Suburban

Number of Studies: 13 Avg. Num. of Vehicle Fueling Positions: 14

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Vehicle Fueling Position

Average Rate	Range of Rates	Standard Deviation
23.26	9.80 - 39.50	8.20







DATA FROM THE ITE TRIP GENERATION HANDBOOK, THIRD EDITION

Table E.36 Pass-By and Non-Pass-By Trips Weekday, PM Peak Period Land Use Code 944—Gasoline/Service Station

SIZE	VEHICLE		WEEKDAY				NON-F	PASS-BY TRIPS	(%)	ADJ. STREET	
(1,000 SQ. FT. GFA)	FUELING POSITIONS	LOCATION	SURVEY DATE	NO. OF INTERVIEWS	TIME PERIOD	PASS-BY TRIP (%)	PRIMARY	DIVERTED	TOTAL	PEAK HOUR VOLUME	SOURCE
_	_	Chicago suburbs, IL	1987	48	3:00-7:00 p.m.	21	_	_	79	_	Kenig, O'Hara, Humes, Flock
_	_	Chicago suburbs, IL	1987	34	3:00–6:00 p.m.	25	_	_	75	_	Kenig, O'Hara, Humes, Flock
_	_	Chicago suburbs, IL	1987	42	3:00–6:00 p.m.	20	_	_	80	_	Kenig, O'Hara, Humes, Flock
2.3	6	Gaithersburg, MD	1992	55	4:00–6:00 p.m.	40	11	49	60	2,760	RBA
2.1	6	Bethesda, MD	1992	30	4:00–6:00 p.m.	53	20	27	47	1,060	RBA
1.7	6	Wheaton, MD	1992	18	4:00–6:00 p.m.	61	6	33	39	2,510	RBA
2.0	8	Gaithersburg, MD	1992	47	4:00–6:00 p.m.	62	23	15	38	2,635	RBA
1.2	6	Damascus, MD	1992	26	4:00–6:00 p.m.	58	11	31	42	1,020	RBA
0.3	12	Wheaton, MD	1992	52	4:00–6:00 p.m.	38	10	52	62	3,835	RBA

Average Pass-By Trip Percentage: 42 "—" means no data were provided

Table E.37 Pass-By and Non-Pass-By Trips Weekday, AM Peak Period Land Use Code 945—Gasoline/Service Station with Convenience Market

SIZE	VEHICLE FUELING		WEEKDAY SURVEY	NO. OF		PASS-BY	NON-P	ASS-BY TRIP	6 (%)	ADJ. STREET PEAK HOUR	
(1,000 SQ. FT. GFA)	POSITIONS	LOCATION	DATE	INTERVIEWS	TIME PERIOD	TRIP (%)	PRIMARY	DIVERTED	TOTAL	VOLUME	SOURCE
0.8	8	Louisville area, KY	1993	61	7:00–9:00 a.m.	60	15	25	40	4,000	Barton- Aschman Assoc.
0.6	8	Louisville, KY	1993	48	7:00–9:00 a.m.	68	13	19	32	1,307	Barton- Aschman Assoc.
0.7	10	Louisville, KY	1993	47	7:00–9:00 a.m.	67	11	22	33	1,105	Barton- Aschman Assoc.
0.7	8	Louisville area, KY	1993	_	7:00–9:00 a.m.	56	22	22	44	1,211	Barton- Aschman Assoc.
0.7	10	Louisville area, KY	1993	_	7:00–9:00 a.m.	46	42	12	54	1,211	Barton- Aschman Assoc.
0.3	_	Louisville area, KY	1993	75	7:00–9:00 a.m.	72	15	13	28	_	Barton- Aschman Assoc.
0.8	8	Silver Spring, MD	1992	36	7:00–9:00 a.m.	47	14	39	53	3,095	RBA
0.4	8	Derwood, MD	1992	46	7:00–9:00 a.m.	75	0	25	25	3,770	RBA
2.2	8	Kensington, MD	1992	31	7:00–9:00 a.m.	47	34	19	53	1,785	RBA
1	8	Silver Spring, MD	1992	35	7:00–9:00 a.m.	78	9	13	22	7,080	RBA

Average Pass-By Trip Percentage: 62 "—" means no data were provided

Figure E.18 Gasoline/Service Station with Convenience Market (945)

Average Pass-ByTrip Percentage vs: 1,000 Sq. Ft. Gross Floor Area

On a: Weekday, AM Peak Period

Number of Studies: 10 Average 1,000 Sq. Ft. GFA: 0.8

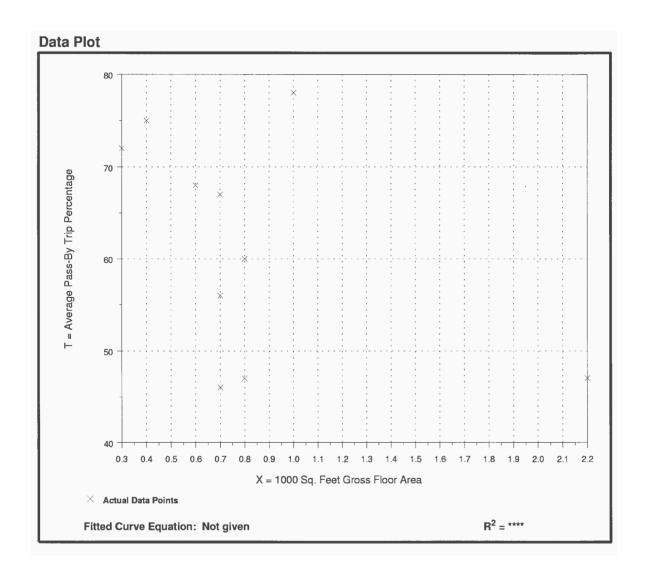




Table E.38 Pass-By and Non-Pass-By Trips Weekday, PM Peak Period Land Use Code 945—Gasoline/Service Station with Convenience Market

SIZE (1,000	VEHICLE		WEEKDAY				NON-P	ASS-BY TRIPS	(%)	ADJ. STREET	
SQ. FT. GFA)	FUELING POSITIONS	LOCATION	SURVEY DATE	NO. OF INTERVIEWS	TIME PERIOD	PASS-BY TRIP (%)	PRIMARY	DIVERTED	TOTAL	PEAK HOUR VOLUME	SOURCE
0.8	8	Louisville area, KY	1993	83	4:00–6:00 p.m.	52	8	40	48	4,965	Barton- Aschman Assoc.
0.6	8	Louisville, KY	1993	60	4:00–6:00 p.m.	53	20	27	47	1,491	Barton- Aschman Assoc.
0.7	10	Louisville, KY	1993	_	4:00–6:00 p.m.	57	19	24	43	1,812	Barton- Aschman Assoc.
0.7	8	Louisville area, KY	1993	_	4:00–6:00 p.m.	72	7	21	28	2,657	Barton- Aschman Assoc.
0.7	10	Louisville area, KY	1993	_	4:00–6:00 p.m.	55	16	29	45	2,657	Barton- Aschman Assoc.
0.8	8	Silver Spring, MD	1992	36	4:00–6:00 p.m.	67	14	19	33	3,095	RBA
0.4	8	Derwood, MD	1992	46	4:00–6:00 p.m.	46	11	43	54	3,770	RBA
2.1	8	Kensington, MD	1992	31	4:00–6:00 p.m.	52	13	35	48	1,785	RBA
1	8	Silver Spring, MD	1992	35	4:00–6:00 p.m.	54	3	43	46	7,080	RBA

Average Pass-By Trip Percentage: 56 "—" means no data were provided

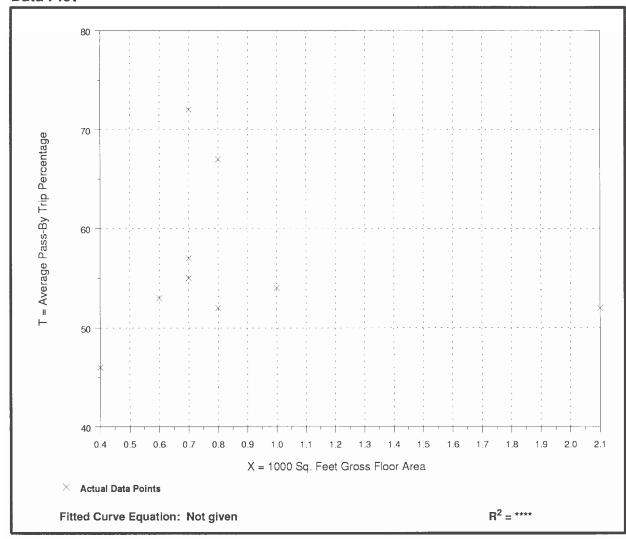
Figure E.19 Gasoline/Service Station with Convenience Market (945)

Average Pass-ByTrip Percentage vs: 1,000 Sq. Ft. Gross Floor Area

On a: Weekday, PM Peak Period

Number of Studies: 9
Average 1,000 Sq. Ft. GFA: 0.9

Data Plot







FUTURE (2027) NO-BUILD CAPACITY REPORTS

Weekday Morning Peak Hour

Weekday Evening Peak Hour

Saturday Midday Peak Hour

Intersection							
Int Delay, s/veh	0.6						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	CDL Š	↑ ↑	↑	WDK	SDL Š	ODK ř	
Traffic Vol, veh/h	45	1165	715	15	15	35	
Future Vol, veh/h	45	1165	715	15	15	35	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	120	-	-	140	0	0	
Veh in Median Storage,		0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	7	7	12	2	6	
Mvmt Flow	47	1226	753	16	16	37	
Major/Minor N	lajor1	N	Major2	N	/linor2		
Conflicting Flow All	769	0	-		1460	377	
Stage 1	-	-	_	-	753	-	
Stage 2	_	<u>-</u>	_	_	707	_	
Critical Hdwy	4.14	-	_	_	6.84	7.02	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	_	-	_	-	5.84	-	
Follow-up Hdwy	2.22	-	-	-	3.52	3.36	
Pot Cap-1 Maneuver	841	-	-	-	120	609	
Stage 1	-	-	-	-	426	-	
Stage 2	-	-	-	-	450	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	841	-	-	-	113	609	
Mov Cap-2 Maneuver	-	-	-	-	245	-	
Stage 1	-	-	-	-	402	-	
Stage 2	-	-	-	-	450	-	
Approach	EB		WB		SB		
HCM Control Delay, s	0.4		0		14.1		
HCM LOS	0.4		- 0		В		
Mineral and Maria Maria		EDI	EDT	MOT	MPP	ODI :: 4 O	N 0
Minor Lane/Major Mvmt		EBL	EBT	WBT	WRK ?	SBLn1 SI	
Capacity (veh/h)		841	-	-	-	245	609
HCM Lane V/C Ratio		0.056	-	-			0.06
HCM Control Delay (s)		9.5	-	-	-	20.7	11.3
HCM Lane LOS		A	-	-	-	С	В
HCM 95th %tile Q(veh)		0.2	-	-	-	0.2	0.2

Intersection							
Int Delay, s/veh	1.2						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	T T	↑ ↑	<u>₩</u>	VVDIX	JDL Š	7	
Traffic Vol., veh/h	80	1105	1440	45	10	80	
Future Vol, veh/h	80	1105	1440	45	10	80	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	- Olop	None	
Storage Length	120	-	_	140	0	0	
Veh in Median Storage		0	0	-	0	-	
Grade, %	-	0	0	_	0	_	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	3	3	2	2	2	2	
Mymt Flow	84	1163	1516	47	11	84	
	· ·					•	
N.A /N.A.				_			
	Major1		Major2		Minor2		
Conflicting Flow All	1563	0	-		2266	758	
Stage 1	-	-	-	-	1516	-	
Stage 2	-	-	-	-	750	-	
Critical Hdwy	4.16	-	-	-	6.84	6.94	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	-	-	-	-	5.84	-	
Follow-up Hdwy	2.23	-	-	-	3.52	3.32	
Pot Cap-1 Maneuver	414	-	-	-	34	350	
Stage 1	-	-	-	-	168	-	
Stage 2	-	-	-	-	427	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	414	-	-	-	27	350	
Mov Cap-2 Maneuver	-	-	-	-	102	-	
Stage 1	-	-	-	-	134	-	
Stage 2	-	-	-	-	427	-	
Approach	EB		WB		SB		
HCM Control Delay, s	1.1		0		21.4		
HCM LOS					С		
Minor Long (Maior M		EDI	EDT	MOT	MDD	ODL 4.0	ייי וחי
Minor Lane/Major Mvm	It	EBL	EBT	WBT	WRK :	SBLn1 S	
Capacity (veh/h)		414	-	-	-	102	350
HCM Lane V/C Ratio		0.203	-	-	-	0.103	
HCM Control Delay (s)		15.9	-	-	-	44.3	18.5
HCM Lane LOS		С	-	-	-	E	С
HCM 95th %tile Q(veh))	0.8	-	-	-	0.3	0.9

Intersection							
Int Delay, s/veh	1.2						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	ሻ	^	^	7	ሻ	7	
Traffic Vol, veh/h	80	1150	1225	25	10	100	
Future Vol, veh/h	80	1150	1225	25	10	100	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	120	-	-	140	0	0	
Veh in Median Storage	e,# -	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	2	2	2	2	4	
Mvmt Flow	84	1211	1289	26	11	105	
Major/Minor I	Major1	<u> </u>	Major2	<u> </u>	Minor2		
Conflicting Flow All	1315	0	-	0	2063	645	
Stage 1	-	-	-	-	1289	-	
Stage 2	-	-	-	-	774	-	
Critical Hdwy	4.14	-	-	-	6.84	6.98	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	-	-	-	-	5.84	-	
Follow-up Hdwy	2.22	-	-	-	3.52	3.34	
Pot Cap-1 Maneuver	522	-	-	-	47	410	
Stage 1	-	-	-	-	222	-	
Stage 2	-	-	-	-	415	-	
Platoon blocked, %		-	-	-			
Mov Cap-1 Maneuver	522	-	-	-	39	410	
Mov Cap-2 Maneuver	-	-	-	-	132	-	
Stage 1	-	-	-	-	186	-	
Stage 2	-	-	-	-	415	-	
Approach	EB		WB		SB		
HCM Control Delay, s	0.9		0		18.4		
HCM LOS					С		
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR S	SBLn1 S	BLn2
Capacity (veh/h)		522	_	-	-	132	410
HCM Lane V/C Ratio		0.161	-	_	_	0.08	
HCM Control Delay (s)		13.2	_	-	_	34.6	16.8
HCM Lane LOS		В	-	-	_	D	С
HCM 95th %tile Q(veh)	0.6	-	-	-	0.3	1



FUTURE (2027) BUILD CAPACITY REPORTS

Weekday Morning Peak Hour

Weekday Evening Peak Hour

Saturday Midday Peak Hour

Intersection							
Int Delay, s/veh	1.8						
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	CDL	↑ ↑	<u>₩</u>	WDK 7	SDL	JDK 7	
Traffic Vol, veh/h	90	1150	595	170	40	185	
Future Vol, veh/h	90	1150	595	170	40	185	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	120	-	-	140	0	0	
Veh in Median Storage,	# -	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	7	7	12	2	6	
Mvmt Flow	95	1211	626	179	42	195	
Major/Minor M	1ajor1	N	Major2	N	/linor2		
Conflicting Flow All	805	0	-		1422	313	
Stage 1	-	-	-	-	626	-	
Stage 2	-	-	-	-	796	-	
Critical Hdwy	4.14	-	-	-	6.84	7.02	
Critical Hdwy Stg 1	-	-	-	-	5.84	-	
Critical Hdwy Stg 2	-	-	-	-	5.84	-	
Follow-up Hdwy	2.22	-	-	-	3.52	3.36	
Pot Cap-1 Maneuver	815	-	-	-	127	671	
Stage 1	-	-	-	-	495	-	
Stage 2	-	-	-	-	405	-	
Platoon blocked, %	0.15	-	-	-	4.0	0= 1	
Mov Cap-1 Maneuver	815	-	-	-	112	671	
Mov Cap-2 Maneuver	-	-	-	-	243	-	
Stage 1	-	-	-	-	437	-	
Stage 2	-	-	-	-	405	-	
Approach	EB		WB		SB		
HCM Control Delay, s	0.7		0		14.3		
HCM LOS					В		
Minor Lane/Major Mvmt		EBL	EBT	WBT	WBR	SBLn1 S	BLn2
Capacity (veh/h)		815	-	-	_	243	671
HCM Lane V/C Ratio		0.116	-	-	_	0.173	0.29
HCM Control Delay (s)		10	-	-	-	22.9	12.5
HCM Lane LOS		A	-	-	-	C	В
HCM 95th %tile Q(veh)		0.4	-	-	-	0.6	1.2

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	NDL N	7	1	ווטוז	ODL	4
Traffic Vol, veh/h	1	<u>r</u> 1	100	1	1	6 5
Future Vol, veh/h	1		100			65
	1	1		1	1	
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	0	-	-	-	-
Veh in Median Storage		-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	95	95	95	95	95	95
Heavy Vehicles, %	2	2	5	2	2	4
Mvmt Flow	1	1	105	1	1	68
Major/Minor	Minor1	N	Major1	1	Major2	
Conflicting Flow All	176	106	0	0	106	0
Stage 1	106	-	-	-	-	-
Stage 2	70	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	_	_	_	_	_
Critical Hdwy Stg 2	5.42	_	_	_	_	_
Follow-up Hdwy	3.518		_	_	2.218	_
Pot Cap-1 Maneuver	814	948	_	_	1485	_
	918			_	1403	
Stage 1		-	-	-	-	-
Stage 2	953	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	813	948	-	-	1485	-
Mov Cap-2 Maneuver	813	-	-		-	-
Stage 1	918	-	-	-	-	-
Stage 2	952	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	9.1		0		0.1	
HCM LOS	Α					
Minor Long/Major Mars	at .	NDT	NDDV	\/DI ∽4\/	VDI 20	CDI
Minor Lane/Major Mvn	ι	NBT		VBLn1V		SBL
Capacity (veh/h)		-	-	813	948	1485
HCM Lane V/C Ratio		-	-	0.001		
HCM Control Delay (s)		-	-	9.4	8.8	7.4
HCM Lane LOS		-	-	Α	Α	Α
HCM 95th %tile Q(veh)	-	-	0	0	0
	•					

Intersection						
Int Delay, s/veh	4.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	VVDL	VVDK	IND I	INDIX	ODL	<u>उठा</u>
Traffic Vol, veh/h	175	40	6 0	200	15	5 0
Future Vol, veh/h	175	40	60	200	15	50
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	0	-	0	_	-
Veh in Median Storage	, # 0	-	0	_	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	95	95	95	95	95	95
Heavy Vehicles, %	2	2	5	2	2	4
Mvmt Flow	184	42	63	211	16	53
Major/Minor I	Minor1	N	/lajor1		Major2	
Conflicting Flow All	148	63	0	0	274	0
Stage 1	63	-	-	U	2/4	-
Stage 2	85	-	-	-	-	_
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	0.22	_	_	4.12	_
Critical Hdwy Stg 1	5.42	-				
Follow-up Hdwy	3.518	3.318	_	_		_
Pot Cap-1 Maneuver	844	1002	_	_	1289	_
Stage 1	960	-	_	_	1200	_
Stage 2	938	_	_	_	_	_
Platoon blocked, %	300		_	_		_
Mov Cap-1 Maneuver	833	1002	_	_	1289	_
Mov Cap-2 Maneuver	833	-	_	_	1205	_
Stage 1	960	_	_	_	_	_
Stage 2	926	<u>-</u>	_	_	_	_
Olage 2	320					
Approach	WB		NB		SB	
HCM Control Delay, s	10.2		0		1.8	
HCM LOS	В					
Minor Lane/Major Mvm	nt	NBT	NBRV	VBLn1V	VBLn2	SBL
Capacity (veh/h)		-	-			1289
HCM Lane V/C Ratio		-	-	0.221		
HCM Control Delay (s)		-	-	10.5	8.8	7.8
HCM Lane LOS		-	-	В	Α	Α
HCM 95th %tile Q(veh))	-	-	0.8	0.1	0

Intersection								
Int Delay, s/veh	7.5							
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		^	^	7	ች	7		
Traffic Vol, veh/h	115	1095	1350	170	30	195		
Future Vol, veh/h	115	1095	1350	170	30	195		
Conflicting Peds, #/hr	0	0	0	0	0	0		
Sign Control	Free	Free	Free	Free	Stop	Stop		
RT Channelized	_			None	_	None		
Storage Length	120	-	-	140	0	0		
Veh in Median Storage		0	0		0	_		
Grade, %	- -	0	0	_	0	_		
Peak Hour Factor	95	95	95	95	95	95		
leavy Vehicles, %	3	3	2	2	2	2		
Nymt Flow	121	1153	1421	179	32	205		
VIVIIIL I IOVV	121	1100	1741	113	32	200		
Major/Minor	Major1	N	Major2	ı	Minor2			
Conflicting Flow All	1600	0	- viajoiz	0	2240	711		
Stage 1	1000	-		-	1421	- 11		
Stage 2	-	-	-	_	819	-		
Critical Hdwy	4.16	-	-		6.84	6.94		
	4.10	-	_	-				
critical Hdwy Stg 1	-	-	-	-	5.84	-		
Critical Hdwy Stg 2	- 0.00	-	-	-	5.84	2 22		
Follow-up Hdwy	2.23	-	-	-	3.52	3.32		
Pot Cap-1 Maneuver	401	-	-	-	36	375		
Stage 1	-	-	-	-	189	-		
Stage 2	-	-	-	-	394	-		
Platoon blocked, %		-	-	-		0=-		
Mov Cap-1 Maneuver	401	-	-	-	~ 25	375		
Mov Cap-2 Maneuver	-	-	-	-	~ 25	-		
Stage 1	-	-	-	-	132	-		
Stage 2	-	-	-	-	394	-		
Approach	EB		WB		SB			
HCM Control Delay, s	1.7		0		88.9			
HCM LOS					F			
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR	SBLn1	SBLn2	
Capacity (veh/h)		401	_	_	_	25	375	
HCM Lane V/C Ratio		0.302	-	-	_	1.263		
HCM Control Delay (s)		17.8	_	_		500.4	25.6	
HCM Lane LOS		С	_	_	-	F	D	
HCM 95th %tile Q(veh)	1.3	-	-	_	3.9	3.2	
•	,					J.0	<u> </u>	
lotes	.,	Φ. 5	_		20		1 C N 1 D C :	* All
-: Volume exceeds ca	pacity	\$: De	elay exc	ceeds 3	UUs	+: Com	putation Not Defined	*: All major volume in platoon

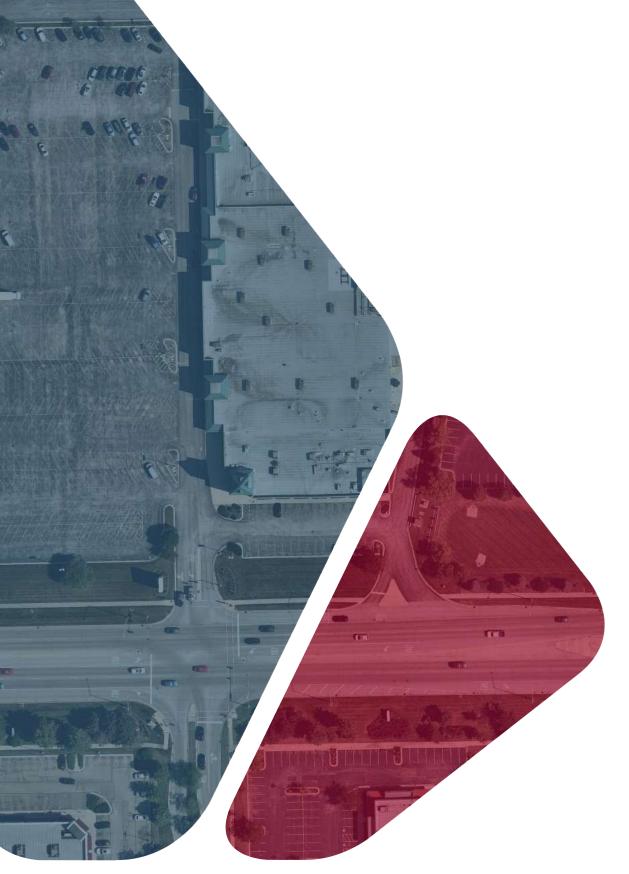
Intersection							
Int Delay, s/veh	0.1						
•		WDD	NDT	NDD	CDI	CDT	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	\	7	♣		4	<u>र्</u> स	
Traffic Vol, veh/h	1	1	165	1	1	105	
Future Vol, veh/h	1	1	165	1	1	105	
Conflicting Peds, #/hr	0	0	_ 0	_ 0	_ 0	_ 0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	0	0	-	-	-	-	
Veh in Median Storage	e, # 0	-	0	-	-	0	
Grade, %	0	-	0	-	-	0	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	2	2	2	2	2	
Mvmt Flow	1	1	174	1	1	111	
		_		_			
	Minor1		/lajor1		Major2		
Conflicting Flow All	288	175	0	0	175	0	
Stage 1	175	-	-	-	-	-	
Stage 2	113	-	-	-	-	-	
Critical Hdwy	6.42	6.22	-	-	4.12	-	
Critical Hdwy Stg 1	5.42	-	-	-	-	-	
Critical Hdwy Stg 2	5.42	-	-	-	_	-	
Follow-up Hdwy		3.318	-	-	2.218	-	
Pot Cap-1 Maneuver	702	868	-	-	1401	-	
Stage 1	855	-	_	-	_	_	
Stage 2	912	_	_	_	_	_	
Platoon blocked, %	012		_	_		_	
Mov Cap-1 Maneuver	701	868	_	_	1401	_	
Mov Cap-1 Maneuver	701	- 000	_	_	1401	_	
· · · · · · · · · · · · · · · · · · ·	855		_	_	<u>-</u>	<u>-</u>	
Stage 1		-	-	_	-	_	
Stage 2	911	-	-	-	-	-	
Approach	WB		NB		SB		
HCM Control Delay, s	9.6		0		0.1		
HCM LOS	A						
	, ,						
Minor Lane/Major Mvn	nt	NBT	NBRV	VBLn1V	VBLn2	SBL	
Capacity (veh/h)		-	-	701	868	1401	
HCM Lane V/C Ratio		-	-	0.002	0.001	0.001	
HCM Control Delay (s)		_	-	10.1	9.2	7.6	
HCM Lane LOS		_	-	В	Α	Α	
HCM 95th %tile Q(veh)	_	_	0	0	0	
	1			J	J	v	

Intersection							
Int Delay, s/veh	3.5						
		WED	NDT	NDD	CDI	CDT	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	ነሻ	7	105	100	4.5	4	
Traffic Vol, veh/h	135	40	125	160	15	90	
Future Vol, veh/h	135	40	125	160	15	90	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	0	0	-	0	-	-	
Veh in Median Storage	e, # 0	-	0	-	-	0	
Grade, %	0	-	0	-	-	0	
Peak Hour Factor	95	95	95	95	95	95	
Heavy Vehicles, %	2	2	2	2	2	2	
Mvmt Flow	142	42	132	168	16	95	
NA -:/NA:	N 4: 4		1-11		M-:0		
	Minor1		Major1		Major2		
Conflicting Flow All	259	132	0	0	300	0	
Stage 1	132	-	-	-	-	-	
Stage 2	127	-	-	-	-	-	
Critical Hdwy	6.42	6.22	-	-	4.12	-	
Critical Hdwy Stg 1	5.42	-	-	-	-	-	
Critical Hdwy Stg 2	5.42	-	-	-	-	-	
Follow-up Hdwy		3.318	-	-	2.218	-	
Pot Cap-1 Maneuver	730	917	-	-	1261	-	
Stage 1	894	-	-	-	-	-	
Stage 2	899	-	-	-	-	-	
Platoon blocked, %			-	-		-	
Mov Cap-1 Maneuver	721	917	-	-	1261	-	
Mov Cap-2 Maneuver	721	-	-	-	-	-	
Stage 1	894	-	-	-	-	-	
Stage 2	887	_	_	_	_	_	
Jugo 2	301						
Approach	WB		NB		SB		
HCM Control Delay, s	10.7		0		1.1		
HCM LOS	В						
Minor Lane/Major Mvm	nt	NBT	NRRV	VBLn1V	VRI n2	SBL	
	π	וטוו	אוטויו				
Capacity (veh/h)		-	-	721	917	1261	
HCM Cartral Dalay (2)		-		0.197			
HCM Control Delay (s)		-	-	11.2	9.1	7.9	
HCM Lane LOS	,	-	-	В	A	A	
HCM 95th %tile Q(veh)	-	-	0.7	0.1	0	

5.1						
	EDT	WDT	WDD	CDI	CDD	
	INOHE					
	0					
π -						
95						
121	1200	1100	100	UZ	220	
		Major2				
1353	0	-	0		598	
-	-	-	-		-	
-	-	-	-		-	
4.14	-	-	_	6.84	6.98	
-	-	-	-		-	
-	-	-	-		-	
	-	-	-			
504	-	-	-		440	
-	-	-	-		-	
-	-	-	-	383	-	
	-	-	-			
504	-	-	-		440	
-	-	-	-		-	
-	-	-	-		-	
-	-	-	-	383	-	
EB		WB		SB		
1.0		U		-		
			14/5-	14/55	0DL (201 2
		EBT	WBT	WBR		
	504	-	-	-	37	440
		-	-	-		
		-	-	-		21.5
						_
	0.9	-	-	-	F 3.1	2.9
	115 115 0 Free - 120 # - 95 2 121 Major1 1353 - 4.14 - 2.22 504 - 504	EBL EBT 115 1140 115 1140 0 0 Free Free - None 120 - # - 0 95 95 2 2 121 1200 Major1 N 1353 0 504 504 504 504 EB 1.3	EBL EBT WBT 115 1140 1135 115 1140 1135 0 0 0 Free Free Free - None - - 120 - - # - 0 0 95 95 95 2 2 2 121 1200 1195 Major1 Major2 1353 0	EBL EBT WBT WBR 115 1140 1135 150 0 0 0 0 Free Free Free Free - None - None 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 140 # - 0 0 - 158 Major1 Major2 Major2 1353 0 - 0 0 - 0 - 0 4.14 <td>EBL EBT WBT WBR SBL 115 1140 1135 150 30 115 1140 1135 150 30 0 0 0 0 0 Free Free Free Free Stop - None - None - 140 0 # - 0 0 - 0 0 0 0 95 9</td> <td>EBL EBT WBT WBR SBL SBR 115 1140 1135 150 30 215 115 1140 1135 150 30 215 0 0 0 0 0 0 Free Free Free Stop Stop - None - None - None - None 120 - 140 0 0 # - 0 0 - 0 - 0 - 0 0 - 0 - 0 95 95 95 95 95 2 2 2 2 2 2 4 121 1200 1195 158 32 226 226 Major1 Major2 Minor2 Minor2 2 2 2 2 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4</td>	EBL EBT WBT WBR SBL 115 1140 1135 150 30 115 1140 1135 150 30 0 0 0 0 0 Free Free Free Free Stop - None - None - 140 0 # - 0 0 - 0 0 0 0 95 9	EBL EBT WBT WBR SBL SBR 115 1140 1135 150 30 215 115 1140 1135 150 30 215 0 0 0 0 0 0 Free Free Free Stop Stop - None - None - None - None 120 - 140 0 0 # - 0 0 - 0 - 0 - 0 0 - 0 - 0 95 95 95 95 95 2 2 2 2 2 2 4 121 1200 1195 158 32 226 226 Major1 Major2 Minor2 Minor2 2 2 2 2 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4

Int Delay, s/veh	Intersection							
Movement WBL WBR NBT NBR SBL SBT		0.1						
Traffic Vol, veh/h		\M/RI	WRR	NRT	NRR	SRI	SRT	
Traffic Vol, veh/h 1 1 145 1 1 125 Future Vol, veh/h 1 1 145 1 1 125 Conflicting Peds, #/hr 0 0 0 0 0 0 0 Sign Control Stop Stop Free By<					אטוז	ODL		
Future Vol, veh/h 1 1 145 1 1 125 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free					1	1		
Conflicting Peds, #/hr		-	•					
Sign Control Stop RT Channelized Stop None Free Free Free Free Free Free RT Channelized - None - None - None - None None <th< td=""><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td>•</td><td></td><td></td><td></td><td></td><td></td></th<>	· · · · · · · · · · · · · · · · · · ·		•					
RT Channelized - None - None - None - None Storage Length 0 0								
Storage Length								
Veh in Median Storage, # 0 - 0 - - 0 Grade, % 0 - 0 - - 0 Peak Hour Factor 95 95 95 95 95 95 Heavy Vehicles, % 2 2 2 2 2 2 2 4 Mvmt Flow 1 1 153 1 1 132 Major/Minor Minor Major Major Major 1 1 132 Major/Minor Minor 1 Major 1 4 1 - - - - - - - -				-	None		None	
Grade, % 0 - 0 - - 0 Peak Hour Factor 95 4 132 132 1426 0 154 0 0 154 0 0 1412 - - - - - - - - - - - - - - - - - <td></td> <td></td> <td></td> <td>_</td> <td>-</td> <td></td> <td>_</td> <td></td>				_	-		_	
Peak Hour Factor 95 96								
Heavy Vehicles, % 2 2 2 2 2 4								
Mymt Flow 1 1 153 1 1 132 Major/Minor Minor1 Major1 Major2 Conflicting Flow All 288 154 0 0 154 0 Stage 1 154 - - - - - - Stage 2 134 -								
Major/Minor Minor1 Major1 Major2 Conflicting Flow All 288 154 0 0 154 0 Stage 1 154 - - - - - Stage 2 134 - - - - - Critical Hdwy 6.42 6.22 - 4.12 - <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								
Conflicting Flow All 288 154 0 0 154 0 Stage 1 154 - - - - - Stage 2 134 - - - - - Critical Hdwy 6.42 6.22 - 4.12 - Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 - 2.218 - Pot Cap-1 Maneuver 702 892 - 1426 - Stage 1 874 - - - - Stage 2 892 - - 1426 - Mov Cap-1 Maneuver 701 892 - 1426 - Mov Cap-2 Maneuver 701 - - - - Stage 1 874 - - - -	Mvmt Flow	1	1	153	1	1	132	
Conflicting Flow All 288 154 0 0 154 0 Stage 1 154 - - - - - Stage 2 134 - - - - - Critical Hdwy 6.42 6.22 - 4.12 - Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 - 2.218 - Pot Cap-1 Maneuver 702 892 - 1426 - Stage 1 874 - - - - Mov Cap-1 Maneuver 701 892 - 1426 - Mov Cap-2 Maneuver 701 - - - - Stage 2 891 - - - - Approach WB NB SB HCM Control Delay, s								
Conflicting Flow All 288 154 0 0 154 0 Stage 1 154 - - - - - Stage 2 134 - - - - - Critical Hdwy 6.42 6.22 - 4.12 - Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 - 2.218 - Pot Cap-1 Maneuver 702 892 - 1426 - Stage 1 874 - - - - Stage 2 892 - - 1426 - Mov Cap-1 Maneuver 701 892 - 1426 - Mov Cap-2 Maneuver 701 - - - - Stage 1 874 - - - -	Major/Minor I	Minor1	N	Maior1		Maior2		
Stage 1 154 - - - - Stage 2 134 - - - - Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - Follow-up Hdwy 3.518 3.318 - - 2.218 - Follow-up Hdwy 3.518 3.318 - - 2.218 - Pot Cap-1 Maneuver 702 892 - - 1426 - Stage 1 874 - - - - - - Mov Cap-1 Maneuver 701 892 - 1426 - Mov Cap-2 Maneuver 701 - - - - Stage 1 874 - - - - Stage 2 891 - - - - Approach WB NB SB HCM LOS							0	
Stage 2 134 -								
Critical Hdwy 6.42 6.22 - 4.12 - Critical Hdwy Stg 1 5.42 - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 - - 2.218 - Pot Cap-1 Maneuver 702 892 - - 1426 - Stage 1 874 - - - - - Stage 2 892 - - - - - Mov Cap-1 Maneuver 701 892 - 1426 - Mov Cap-2 Maneuver 701 - - - - Stage 1 874 - - - - Stage 2 891 - - - - Approach WB NB SB HCM Control Delay, s 9.5 0 0.1 Minor Lane/Major Mvmt NBT	•							
Critical Hdwy Stg 1 5.42								
Critical Hdwy Stg 2 5.42 -					_			
Follow-up Hdwy 3.518 3.318 2.218 - Pot Cap-1 Maneuver 702 892 1426 - Stage 1 874 Stage 2 892 Platoon blocked, % Mov Cap-1 Maneuver 701 892 1426 - Mov Cap-2 Maneuver 701 Stage 1 874 Stage 2 891 Approach WB NB SB HCM Control Delay, s 9.5 HCM LOS A Minor Lane/Major Mvmt NBT NBRWBLn1WBLn2 SBL Capacity (veh/h) - 701 892 1426 HCM Lane V/C Ratio - 0.002 0.001 0.001 HCM Control Delay (s) - 10.1 9 7.5 HCM Lane LOS - B A				-	_			
Pot Cap-1 Maneuver 702 892 - - 1426 - Stage 1 874 - - - - - Stage 2 892 - - - - - Platoon blocked, % -				_	_			
Stage 1 874 -					_			
Stage 2 892 -	•				-			
Platoon blocked, %					-			
Mov Cap-1 Maneuver 701 892 - - 1426 - Mov Cap-2 Maneuver 701 - <td></td> <td>892</td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td>		892	-		-	-		
Mov Cap-2 Maneuver 701 -		704	000		-	4.400		
Stage 1 874 -								
Stage 2 891 -			-	-	-	-	-	
Approach WB NB SB HCM Control Delay, s 9.5 0 0.1 HCM LOS A Minor Lane/Major Mvmt NBT NBRWBLn1WBLn2 SBL Capacity (veh/h) - - 701 892 1426 HCM Lane V/C Ratio - - 0.002 0.001 0.001 HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - B A A	•		-	-	-	-	-	
HCM Control Delay, s 9.5 0 0.1 HCM LOS	Stage 2	891	-	-	-	-	-	
HCM Control Delay, s 9.5 0 0.1 HCM LOS								
HCM Control Delay, s 9.5 0 0.1	Approach	WB		NB		SB		
Minor Lane/Major Mvmt NBT NBRWBLn1WBLn2 SBL Capacity (veh/h) - - 701 892 1426 HCM Lane V/C Ratio - - 0.002 0.001 0.001 HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - - B A A								
Minor Lane/Major Mvmt NBT NBRWBLn1WBLn2 SBL Capacity (veh/h) - - 701 892 1426 HCM Lane V/C Ratio - - 0.002 0.001 0.001 HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - B A A				U		0.1		
Capacity (veh/h) - - 701 892 1426 HCM Lane V/C Ratio - - 0.002 0.001 0.001 HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - - B A A	TIOW LOO	٨						
Capacity (veh/h) - - 701 892 1426 HCM Lane V/C Ratio - - 0.002 0.001 0.001 HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - B A A	Minor Lane/Major Mym	nt	NRT	NRRV	VRI n1V	VRI n2	SRI	
HCM Lane V/C Ratio - - 0.002 0.001 0.001 HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - B A A		i i (INDT	NDIXV				
HCM Control Delay (s) - - 10.1 9 7.5 HCM Lane LOS - - B A A			-	-				
HCM Lane LOS B A A								
)						
11014 0511 0/11 0/ 1)		,	-	-				
HCM 95th %tile Q(veh) 0 0 0	HCM 95th %tile Q(veh)	1)	-	-	0	0	0	

Intersection						
Int Delay, s/veh	3.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	ሻ	7	<u> </u>	7	ODL	4
Traffic Vol, veh/h	135	40	105	160	15	110
Future Vol, veh/h	135	40	105	160	15	110
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	0	_	0	_	-
Veh in Median Storage		-	0	_	_	0
Grade, %	0	_	0	_	_	0
Peak Hour Factor	95	95	95	95	95	95
Heavy Vehicles, %	2	2	2	2	2	4
Mymt Flow	142	42	111	168	16	116
WWIIICI IOW	ITL	72	111	100	10	110
	Minor1		Major1		Major2	
Conflicting Flow All	259	111	0	0	279	0
Stage 1	111	-	-	-	-	-
Stage 2	148	-	-	-	-	-
Critical Hdwy	6.42	6.22	-	-	4.12	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	-	-		-
Pot Cap-1 Maneuver	730	942	-	-	1284	-
Stage 1	914	-	-	-	-	-
Stage 2	880	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	721	942	-	-	1284	-
Mov Cap-2 Maneuver	721	-	-	-	-	-
Stage 1	914	-	-	-	-	-
Stage 2	869	-	-	-	-	-
Approach	WB		NB		SB	
	10.7		0		0.9	
HCM Control Delay, s HCM LOS			U		0.9	
HCIVI LUS	В					
Minor Lane/Major Mvm	nt	NBT	NBRV	VBLn1V	VBLn2	SBL
Capacity (veh/h)		-	-	721	942	1284
HCM Lane V/C Ratio		-	-	0.197		
HCM Control Delay (s)		-	-	11.2	9	7.8
HCM Lane LOS		-	-	В	Α	Α
HCM 95th %tile Q(veh))	-	-	0.7	0.1	0







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